SUMMARY
OF
RESEARCH REPORT

SHELTER ENVIRONMENTAL PREDICTION (SHEP)

COMPUTER CODE

MODIFICATION 3

USER'S MANUAL

GARD Final Report 1423 June 1968

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General American Research Division
General American Transportation Corporation

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INTRODUCTION

The Shelter Environmental Prediction (SHEP) computer code will calculate the environmental response of a shelter, or any large structure, to time-varying thermal loads and ventilation inlet psychrometric conditions. Shelter conditions computed by finite difference methods define the history of the shelter environment during occupancy.

The SHEP code accommodates solar radiation, boundary surface heat transfer, moisture evaporation or condensation on the boundaries, equipment and lighting loads, and air conditioning. Little technical knowledge of mass or energy transfer is required by a user of the SHEP code. Information that must be supplied to the code includes shelter physical, thermal and geometrical characteristics, occupancy levels and durations, and hourly inlet conditions.

The shelter model used in the code is based upon the assumptions that:

1. Air within the shelter and ventilation air is completely and instantaneously mixed, so that one psychrometric condition will completely specify the shelter environment;

2. Moisture condensation and evaporation is filmwise with the convective heat transfer coefficients constant over each boundary surface, but variable from boundary to boundary.

3. Radiative energy transfer between the shelter boundaries is neglected.

4. Shelter exhaust air is at the psychrometric condition of the shelter atmosphere; and

5. Thermal and physical properties of the air and of the structural materials are not temperature-dependent.
The SHEP code permits the analysis of an actual shelter with up to 20 different boundaries, enclosing a volume which the sensible and latent energy exchange with the environment external to the shelter.

The user's manual explains the various features of the SHEP code, presents the input and output formats, gives representative input data values, and includes an application of the code to a typical shelter structure.

The code is written in FORTRAN IV specifically for the CDC 3600 computer system and consists of 78 cards. It requires a memory bank of at least \(65^k\) words (each word of 48 bits) for the code and the accompanying matrices.

FEATURES OF THE PROGRAM

The shelter model used by the SHEP code is an accurate description of the actual shelter under analysis because of the methods which have been formulated in the code to handle the thermal processes which affect the shelter environment. These processes include:

1. solar radiation,
2. air conditioning,
3. moisture evaporation and condensation,
4. time-varying inlet conditions, and
5. boundary heat transfer.

It has been found that during extreme hot weather, many actual shelters respond as if they had adiabatic boundaries. Thus, the code has the ability of analyzing a shelter with adiabatic or non-adiabatic shelter boundaries.

Shelter Boundaries

An actual shelter is bounded by walls, floor and ceiling, composed of several different kinds of materials (e.g., cement, glass, metal, etc.) and
these can be at any orientation (slope and azimuth). In addition, the exterior boundary surface may be exposed to various media (e.g., air, soil, etc.). An implicit finite-difference approach based upon a one-dimensional node array is used to compute temperature distribution across a boundary. This nodal point approach to the temperature profile across the boundary permits an implicit representation of the temperature through the boundary by applying an energy balance at each of n nodes. The heat transfer through a non-adiabatic boundary due to conduction may then be computed based on the interior boundary surface temperatures. This implicit procedure does not have the stability considerations associated with the explicit method. Thus, longer time intervals can be utilized at each finite difference increment.

If the boundaries are considered adiabatic, heat transfer both through the boundary and due to condensation or evaporation on the surface are considered zero.

Solar Radiation

If a surface is exposed to ambient air, it will normally be exposed to direct, diffuse and/or reflected solar radiation. If the surface is a shelter boundary, the incident radiation will serve to raise the shelter temperature in two ways. First, incident radiation will be partially absorbed by the boundary, thus raising its temperature and, in time, the temperature of the shelter. Second, radiation transmitted through the boundary will be incident on interior surfaces, similarly raising their temperatures and that of the shelter atmosphere.

SHEP makes several simplifying assumptions in treating the effects of solar radiation. First, incident radiation absorbed by each boundary is
considered a surface phenomenon. Second, all reflected radiation, both that which falls onto the shelter surfaces from surrounding objects and that which is reflected from the shelter surfaces, is neglected. Also, radiation transmitted through a boundary is considered an instantaneous thermal load inside the shelter, similar to the lighting and equipment loads.

**Air Conditioning**

In a typical air conditioning unit, warm air passes over cooling coils, thereby lowering its dry-bulb temperature through convective heat exchange and lowering its moisture content through condensation. The temperature of the coils is not constant, but varies as a function of load. Typically, all the air passing through the air conditioner does not experience these heat and mass transfer processes due to flow turbulence.

The method the SHEP code utilizes to calculate the air conditioning load assumes that the temperature of the coils and the percentage of air unaffected by passing through the unit do not vary with the cooling load. An "effective coil surface temperature" is assumed as the design temperature of the coils; and a "coil bypass factor" is the design value of the percentage of air unaffected by the cooling units. If these two parameters are both assumed constant, the air conditioning performance of an actual unit can be estimated reasonably well.

The ventilation rates of outside air entering the system, of air passing through the air conditioning unit, and of air entering the shelter must all be specified by the code user. Therefore, the mixing processes can be altered, or even eliminated, by varying the various ventilation rates.

Air conditioning removes both sensible and latent energy. This energy removal, $\Delta Q$, is given by
\[ \Delta Q = c_p \dot{m} \Delta T + h_{fg} \dot{m} \Delta W \]

where

- \( c_p \) = specific heat of air \( 0.24 \text{ Btu/lb} \cdot ^\circ\text{F} \)
- \( \dot{m} \) = mass flow rate of dry air through the air conditioning unit, lb/hr
- \( \Delta T \) = temperature difference across the unit, °F
- \( h_{fg} \) = heat of condensation of water vapor, Btu/lb water
- \( \Delta W \) = humidity ratio difference across the unit, lb water/lb dry air

**Moisture Condensation**

Whenever the vapor pressure at the interior surface of a boundary is lower than the vapor pressure of the shelter atmosphere, moisture will migrate to and condense on the surface, thereby removing energy from the shelter environment. If, at another time, the vapor pressure at the boundary surface is higher than the vapor pressure of the shelter air, the process will be reversed and condensed water on the surface will re-evaporate and migrate into the shelter atmosphere.

If sufficient moisture condenses, it will run down the walls and accumulate on the floor of the shelter. Since the SHEP code assumes that condensation occurs in an even film on an interior surface, the effect of gravity is neglected.

The amount of energy transfer due to moisture condensation is given by

\[ Q_{\text{condensation}} = 2.825 \frac{\lambda h}{\rho_a} \left( \frac{p_o}{p_b - p_o} - \frac{p_s}{p_b - p_s} \right) \]

where

- \( \lambda \) = heat of condensation
- \( h \) = film heat transfer coefficient
\( \rho_a = \) density of dry air

\( p_o = \) partial pressure of water vapor at shelter temperature

\( p_b = \) barometric pressure

\( p_s = \) partial pressure of water vapor at wall temperature

Evaporation is assumed to be the exact opposite of condensation and, therefore, the same equation applies.

**Metabolic Loads**

The metabolic expressions of Houghten are adopted in this study, since they reflect effects of relative humidity in the shelter. They are given by

\[
Q_{\text{sensible}} = -0.06875(T_{\text{db}})^2 + 1.625(T_{\text{db}}) + 523.0 \quad \text{for } T_{\text{db}} \geq 50^\circ F
\]

\[
Q_{\text{sensible}} = -1.482 \times ET + 514.0 \quad \text{for } 50^\circ F \leq ET \leq 87^\circ F
\]

\[
Q_{\text{total}} = \begin{cases} 
-1.508 \times (ET)^2 + 259.7 \times ET - 10795.2 & \text{for } 87^\circ F < ET \leq 102^\circ F \\
0.0 \text{ (assumed)} & \text{for } ET > 102^\circ F
\end{cases}
\]

with \( Q_{\text{latent}} = Q_{\text{total}} - Q_{\text{sensible}} \), assuming that the body is in thermal equilibrium with the shelter environment, and hence, neglecting the heat storage term.

**Varying Inlet Conditions**

The psychrometric condition of the shelter atmosphere and of the entering ventilation air are considered by the code as a function of dry-bulb temperature and relative humidity, which normally vary with time.

Certain other factors which affect the shelter atmosphere and which normally vary are:

1. the number of occupants,
2. the ventilation rate, and
3. the lighting and equipment loads.

In the code, these factors may have different values for each hour of occupancy.
Determination of Shelter Dry-Bulb Temperature

All thermal loads and enthalpies are computed at the beginning of a time increment based upon an estimate of what the shelter dry-bulb temperature will be. Then the net amount of energy added to the shelter system during that increment is calculated and from it, the shelter dry-bulb temperature. Since the shelter dry-bulb temperature of the increment is initially estimated to be that of the last increment, a more accurate shelter dry-bulb temperature for the increment is computed using an iterative procedure.

Determination of Shelter Effective Temperature

After the shelter dry-bulb temperature for an increment has been computed, wet-bulb temperature is determined via the Carrier equation. Using a linear approximation, the effective temperature is calculated from:

\[
ET = \frac{107.5 T_{db} - 45.2 T_{wb}}{T_{db} - T_{wb} + 62.3}
\]

for

\[
45°F \leq T_{db} \leq 110°F
\]

\[
30°F \leq T_{wb} \leq 110°F
\]

where

\[T_{db} = \text{dry-bulb temperature, } °F\]

\[T_{wb} = \text{wet-bulb temperature, } °F\]

The psychrometric condition of the shelter atmosphere at the beginning of the next increment is then set equal to that at the end of the last increment and calculations for the next increment are begun. When one hour's calculations have been completed, the values for the last increment of the hour are printed out as the conditions at the end of the hour.
INTERPRETATION OF OUTPUT

The output of the SHEP program is a tabulation of the instantaneous values of the thermal loads affecting the shelter and the shelter psychrometric condition for the last increment of each hour of occupancy, see Figure 1. It must be remembered that these values are instantaneous and, while they reflect trends in the shelter system, interpolation between hourly values may be invalid. Also, hourly thermal loads determine the resultant hourly shelter temperature; however, the inverse process (i.e., compute loads from shelter temperature) is not valid. The 3600 computer system printer includes a procedure for rounding output to the format specified. Thus, the thermal loads are rounded in value to the nearest integer.

The air conditioning, boundary and condensation heat loads, when positive, represent energy lost from the shelter system; all other positive loads are energy additions. In the SHEP code, the assumptions associated with the calculations of the air conditioning, moisture condensation, and transmitted solar radiation loads generally lead to conservative estimates of these loads.

Maximum and minimum shelter temperatures and the hours of their occurrence are indicated. Average temperatures are computed for the entire occupancy period, for each full day of occupancy, and for specific intervals determined by the code user.
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**Figure 1** Output of Sample Problem

**GENERAL AMERICAN RESEARCH DIVISION**
A. L. KAPIL
SHELTER ENVIRONMENTAL PREDICTION (SHEP)
COMPUTER CODE
MODIFICATION 3

USER'S MANUAL

GARD Final Report 1423 June 1968

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C. E. Rathmann
R. J. Baschierie

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GENERAL AMERICAN RESEARCH DIVISION
FOREWORD

This user's manual was prepared by the General American Research Division of the General American Transportation Corporation for the Stanford Research Institute under Subcontract No. 11599(6300A-090). It explains in detail the procedure for using the computer code to calculate the response of a shelter to time-varying thermal loads and time-varying ventilation inlet psychrometric conditions. The code is based upon research performed between June 1963 and May 1968 on the Analysis of Shelter Ventilation Requirements which falls in the program area of OCD Work Unit 1215A.

The project was monitored by Mr. F. Allen (then at OCD) and Mr. D. Bettge of OCD, and Messrs. C. Grubb and J. Halsey of SRI.

The authors wish to thank Messrs. H. Moy, M. Lokmanhekim, D. Liddell, and A. Kapil of GARD, Dr. J. Buchanan of OCD, Mr. P. Achenbach and Dr. T. Kusuda of the National Bureau of Standards, Mr. W. Spiegel, Consulting Engineer, and Messrs. F. Hughes-Caley and T. Hori of SRI for their comments and criticism.

The valuable cooperation of the personnel at the OCD computer facility in Olney, Maryland and the Control Data Corporation computer facility in Chicago, Illinois is acknowledged.

It should be noted that the version of the SHEP code presented in this report (Mod. 3) has been superseded by a new modification (Mod. 6). This new code employs a slightly different sequence of calculation to decrease calculation time.
ABSTRACT

The Shelter Environmental Prediction (SHEP) Computer Code, Modification 3, calculates the response of a shelter to time-varying thermal loads and time-varying ventilation inlet psychrometric conditions. The code accommodates solar radiation, boundary surface heat transfer, moisture condensation on the boundaries, equipment and lighting loads, and air conditioning. The manual explains the various features of the code, presents the input and output formats, gives representative input data values, and includes an application of the code to a typical shelter structure.

The required inputs to the code and the outputs obtainable from it are given below:

Inputs

1. Ventilation rate
2. Inlet psychrometric conditions
3. Shelter geometric characteristics
4. Shelter thermal characteristics
5. Shelter latitude, longitude and altitude
6. Period of occupancy

Outputs

1. Hourly temperatures
2. Hourly air conditioning load
3. Hourly boundary heat transfer
4. Hourly metabolic loads
5. Average temperatures (dry-bulb, wet-bulb, effective) for the entire occupancy or specified hours of occupancy
6. Maximum and minimum temperatures (dry-bulb, wet-bulb, effective) during the occupancy.

The code is written in FORTRAN IV specifically for the CDC 3600 computer system and consists of approximately 780 cards. It requires a memory bank of at least $65^k$ words (each word of 48 bits) for the code and the accompanying matrices. For the CDC 3600 and for a problem comparable to the sample problem presented in the text, the compilation time is approximately 1 min., 45 sec. and the execution time approximately 1 sec. for each hour of shelter occupancy.
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SECTION 1
INTRODUCTION

The Shelter Environmental Prediction (SHEP) code will calculate the environmental response of a shelter, or any large structure, to time-varying thermal loads and ventilation inlet psychrometric conditions. Shelter conditions computed by finite difference methods define the history of the shelter environment during occupancy.

The SHEP code accommodates solar radiation, boundary surface heat transfer, moisture evaporation or condensation on the boundaries, equipment and lighting loads, and air conditioning (derivations of the corresponding equations are given in the Appendices). Little technical knowledge of mass or energy transfer is required by a user of the SHEP code. Information that must be supplied includes shelter physical, thermal and geometrical characteristics, occupancy levels and durations, and hourly inlet conditions. The amount of required data is admittedly large, but is necessary so that the SHEP code will remain applicable to a wide variety of shelters.

The shelter model used in the code is based upon the assumptions that:

1. Air within the shelter and ventilation air is completely and instantaneously mixed, so that one psychrometric condition will completely specify the shelter environment;

2. Moisture condensation and evaporation is filmwise with the convective heat transfer coefficients constant over each boundary surface, but variable from boundary to boundary.

3. Radiative energy transfer between the shelter boundaries is neglected.

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1-1
4. Shelter exhaust air is at the psychrometric condition of the
   shelter atmosphere; and
5. Thermal and physical properties of the air and of the structural
   materials are not temperature-dependent.

The SHEP code permits the analysis of an actual shelter with up to 20 different
boundaries, enclosing a volume which has sensible and latent energy exchange
with the environment external to the shelter.

This user's manual explains the various features of the SHEP code, presents
the input and output formats, gives representative input data values, and in-
cludes an application of the code to a typical shelter structure.

The code is written in FORTRAN IV specifically for the CDC 3600 computer
system and consists of approximately 780 cards. It requires a memory bank of
at least \(65^k\) words (each word of 48 bits) for the code and the accompanying
matrices.

For the CDC 3600 and for a problem comparable to the sample problem
presented in the text, the compilation time is approximately 1 min., 45 sec.
and the execution time approximately 1 sec. for each hour of shelter occupancy.
SECTION 2
FEATURES OF THE PROGRAM

The shelter model used by the SHEP code is an accurate description of the actual shelter under analysis because of the methods which have been formulated in the code to handle the thermal processes which affect the shelter environment. These processes include:

1. solar radiation,
2. air conditioning,
3. moisture evaporation and condensation,
4. time-varying inlet conditions, and
5. boundary heat transfer.

It has been found that during extreme hot weather, many actual shelters respond as if they had adiabatic boundaries. Thus, the code has the ability of analyzing a shelter with adiabatic or non-adiabatic shelter boundaries.

The complexity of the code has necessitated the printout of diagnostic error messages. These are included as a safeguard against using illegal variable values, or exceeding the inherent limits of the equations comprising the code.

2.1 Shelter Boundaries

An actual shelter is bounded by walls, floor and ceiling, composed of several different kinds of materials (e.g., cement, glass, metal, etc.) and these can be at any orientation (slope and azimuth). In addition, the exterior boundary surface may be exposed to various media (e.g., air, soil, etc.). Therefore, a "boundary" is defined as a plane or approximately plane curved surface* of the shelter enclosure consisting of a homogeneous inner layer and

*See Appendix E.
successive homogeneous layers exposed to one external medium. If windows are included in one wall of the shelter and this wall is partially underground, then this wall consists of three boundaries (see Figure 2-1). A shelter volume may be defined by up to 20 boundaries. A curvilinear boundary should be considered plane, with its orientation that of the plane tangent to the boundary at its midpoint (see Appendix E).

An implicit finite-difference approach based upon a one-dimensional node array is used to compute temperature distribution across a boundary, with each boundary spanned by up to 40 nodal points. A boundary may consist of up to 5 layers, each having distinct thermal properties and nodal-point spacings. An air space within a boundary and a soil media adjacent to a belowgrade boundary are considered as layers of the respective boundaries. Shelter tests have shown that 10 feet from the exterior boundary surface, the soil temperature is invariant. Thus the soil can be considered as a layer 10 feet thick whose exterior surface is at the undisturbed soil temperature.

Nodal point spacing in a typical boundary consisting of 4 layers is shown in Figure 2-2. Each layer is divided into slab $\Delta x_i$ thick and a nodal point is placed at the center of each slab. The innermost and outermost points are $\Delta x_i/2$ from the next inner nodal point and are placed at the surface of the layer (see Appendix C). It should be noted that there is a nodal point at each surface and at each interface, and that the nodal point numbering is continuous.

The number of nodal points in each layer is

$$n_k = \frac{\text{layer thickness}}{\Delta x_k} + 1$$

which includes the node on the inner surface of the layer. The number of
Figure 2-1  A Typical Shelter Wall Consisting of Three Boundaries

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2-3
Figure 2-2 Typical Nodal Point Arrangement in a Four-layered Boundary
nodal points in a wall excluding the outermost point is $N_{MAX}$, and must be supplied by the programmer. It is given by

$$N_{MAX} = \sum_{layers} n_k$$

and the total number of nodal points is

$$N_j = N_{MAX} + 1$$

Spacing between nodal points should vary inversely with conductivity.

Suggested spacing in soil is one-half to one foot; in structural materials, one inch.

The nodal point approach to the temperature profile across the boundary permits an implicit representation of the temperature through the boundary via the simultaneous linear equations:

$$a_{11}T_1 + a_{12}T_2 = b_1$$
$$a_{21}T_1 + a_{22}T_2 + a_{23}T_3 = b_2$$
$$a_{32}T_2 + a_{33}T_3 + a_{34}T_4 = b_3$$
$$\cdots$$
$$a_{n-1,n-2}T_{n-2} + a_{n-1,n-1}T_{n-1} + a_{n-1,n}T_n = b_{n-1}$$
$$a_{n,n-1}T_{n-1} + a_{n,n}T_n = b_n$$

obtained by applying an energy balance at each of $n$ nodes. The $a$'s are the coefficients of the temperatures at each node and the $b$'s are the heat storage terms, which are time-dependent. In matrix form, the equations become:

$$[A][T] = [B]$$
These equations may be solved for the nodal temperatures:

\[
[T] = [A]^{-1} [B]
\]

and the heat transfer through a non-adiabatic boundary due to conduction may be computed based on the interior boundary surface temperatures. In addition, for non-adiabatic boundaries, heat loss due to moisture condensation or evaporation on the interior boundary surfaces is computed. The derivations of the equations for determining the \([A]\) and \([B]\) coefficients, and those for heat transfer due to condensation, are given in Appendix C. This implicit procedure does not have the stability considerations associated with the explicit method. Thus, longer time intervals can be utilized at each finite difference increment.

If the boundaries are considered adiabatic, heat transfer both through the boundary and due to condensation or evaporation on the surface are considered zero.

2.2 Solar Radiation

If a surface is exposed to ambient air, it will normally be exposed to direct, diffuse and/or reflected solar radiation. If the surface is a shelter boundary, the incident radiation will serve to raise the shelter temperature in two ways. First, incident radiation will be partially absorbed by the boundary, thus raising its temperature and, in time, the temperature of the shelter. Second, radiation transmitted through the boundary will be incident on interior surfaces, similarly raising their temperatures and that of the shelter atmosphere.

SHEEP makes several simplifying assumptions in treating the effects of solar radiation. One of these is that all reflected radiation, both that which falls onto the shelter surfaces from surrounding objects and that which
is reflected from the shelter surfaces, is neglected. Also, radiation transmitted through a boundary is considered an instantaneous thermal load inside the shelter, similar to the lighting and equipment loads.

All calculations involving solar radiation are done using solar time, which differs slightly from Civil Time. The relation may be expressed as

\[
\text{Solar Time} = \text{Civil Time} + \text{Equation of Time} + \Delta_{\text{long}}
\]

Civil Time is that time assigned to a zone covering approximately 15° of longitude; it is the same as Standard Time. Since local time actually does not remain constant within each 15° zone, but varies by four minutes for each degree within the zone, a correction factor, \(\Delta_{\text{long}}\), takes this into account. The Equation of Time is the difference between mean solar time and apparent solar time and is given as the \((12^h - \text{Ephemeris Transit})\). See Reference 1.

Solar time is computed in the program knowing the time of the start of occupancy, the longitude of the shelter, and the first day of occupancy.

Variation of the Equation of Time is shown in Figures 2-3 and the values used in the program are listed in Table I. The daily values of the Equation of Time change slightly from year to year, but the actual values remain within 0.3 min. of those listed (see Reference 2).

Solar radiation intensity is computed once each time increment for each exposed wall. (See Appendix B.) Although radiation will penetrate into a surface a certain distance before being absorbed, the SHEP code assumes this absorption phenomenon is a surface effect. Also, even though the transmittance of the boundary material may vary with incident wavelength, only a total transmittance value is used in the code.
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2.3 Air Conditioning

In a typical air conditioning unit, warm air passes over cooling coils, thereby lowering its dry-bulb temperature through convective heat exchange and lowering its moisture content through condensation. The temperature of the coils is not constant, but varies as a function of load. Typically, all the air passing through the air conditioner does not experience these heat and mass transfer processes due to flow turbulence.

The method the SHEP code utilizes to calculate the air conditioning load assumes that the temperature of the coils and the percentage of air unaffected by passing through the unit do not vary with the cooling load. An "effective coil surface temperature" is assumed as the design temperature of the coils; and a "coil bypass factor" is the design value of the percentage of air unaffected by the cooling units. If these two parameters are both assumed constant, the air conditioning performance of an actual unit can be estimated reasonably well. See Appendix F, which is based upon Reference 3.

A typical air conditioning system for a shelter may be represented by the schematic diagram of Figure 2-4; the various psychrometric states of the air in the system are indicated in the accompanying psychrometric chart. Note that "return air bypass" refers to air not passing through air conditioning unit; "coil bypass factor" is a characteristic of the unit itself. Outside air at state point 1 enters the system and is adiabatically mixed with return air at the shelter condition, S, to create state point 2. A portion of this air passes through the air conditioning unit, exiting with a lower dry-bulb temperature and a low humidity ratio, state point 3, and is then adiabatically mixed with the unconditioned air to give state point 4. Air at this condition is the inlet air to the shelter which is then used to compute the new shelter condition, S'.
The ventilation rates of outside air entering the system, of air passing through the air conditioning unit, and of air entering the shelter must all be specified by the code user. Therefore, the mixing processes can be altered, or even eliminated, by varying the various ventilation rates.

Air conditioning removes both sensible and latent energy. This energy removal, $\Delta Q$, is given by

$$\Delta Q = c_p \dot{m} \Delta T + h_{fg} \dot{m} \Delta W$$

where

- $c_p =$ specific heat of air $\approx 0.24$ Btu/lb °F
- $\dot{m} =$ mass flow rate of dry air through the air conditioning unit, lb/hr
- $\Delta T =$ temperature difference across the unit, °F
- $h_{fg} =$ heat of condensation of water vapor, Btu/lb water
- $\Delta W =$ humidity ratio difference across the unit, lb water/lb dry air

### 2.4 Moisture Condensation

Whenever the vapor pressure at the interior surface of a boundary is lower than the vapor pressure of the shelter atmosphere, moisture will migrate to and condense on the surface, thereby removing energy from the shelter environment. If, at another time, the vapor pressure at the boundary surface is higher than the vapor pressure of the shelter air, the process will be reversed and condensed water on the surface will re-evaporate and migrate into the shelter atmosphere.

If sufficient moisture condenses, it will run down the walls and accumulate on the floor of the shelter. Since the SHEP code assumes that condensation occurs in an even film on an interior surface, the effect of gravity is neglected.
Figure 2-4  Schematic Diagram of a Shelter Air-Conditioning System and the Corresponding Processes on a Skeleton Psychrometric Chart

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2-12
In the code, the vapor pressure at the boundary surface is assumed to be the saturation pressure of water vapor at the temperature of the boundary surface. Values of saturation pressures as a function of dry-bulb temperature (see Table II) are a part of the standard input data. Only the range of temperatures from 50°F to 120°F are considered, since metabolic relations used in the SHEP code are invalid outside of this range.

2.5 Metabolic Loads

The metabolic expressions of Houghton are adopted in this study since they reflect effects of relative humidity in the shelter. They are given by

\[ Q_{\text{sensible}} = -0.06875(T_{\text{db}})^2 + 1.625(T_{\text{db}}) + 523.0 \quad \text{for } T_{\text{db}} \geq 50°F \]

\[ Q_{\text{total}} =\begin{cases} -1.482 (ET) + 514.0 & \text{for } 50°F \leq ET \leq 87°F \\ -1.508 (ET)^2 + 259.7 (ET) - 10785.2 & \text{for } 87°F < ET < 102°F \\ 0.0 \text{ (assumed)} & \text{for } ET > 102°F \end{cases} \]

with \( Q_{\text{latent}} = Q_{\text{total}} - Q_{\text{sensible}} \) assuming that the body is in thermal equilibrium with the shelter environment, and hence, neglecting the heat storage term.

2.6 Auxiliary Loads

Lighting and equipment loads are introduced as inputs and may be time-varying (on an hourly basis).

2.7 Varying Inlet Conditions

The psychrometric condition of the shelter atmosphere and of the entering ventilation air are considered by the code as a function of dry-bulb temperature and relative humidity.

Certain factors which affect the shelter atmosphere normally vary with time; ambient temperature and relative humidity are chief among these. Other factors which may change during occupancy are:

*Superscripts refer to references, p. 7-1.
TABLE II

SATURATION PRESSURE, $P_s$, AS A FUNCTION
OF DRY-BULB TEMPERATURE, $T_{db}$

<table>
<thead>
<tr>
<th>$T_{db}$ *</th>
<th>$P_s$ **</th>
<th>$T_{db}$</th>
<th>$P_s$</th>
<th>$T_{db}$</th>
<th>$P_s$</th>
<th>$T_{db}$</th>
<th>$P_s$</th>
<th>$T_{db}$</th>
<th>$P_s$</th>
</tr>
</thead>
<tbody>
<tr>
<td>50</td>
<td>25.648</td>
<td>64</td>
<td>42.494</td>
<td>78</td>
<td>68.357</td>
<td>92</td>
<td>107.021</td>
<td>106</td>
<td>163.368</td>
</tr>
<tr>
<td>51</td>
<td>26.620</td>
<td>65</td>
<td>44.006</td>
<td>79</td>
<td>70.646</td>
<td>93</td>
<td>110.390</td>
<td>107</td>
<td>168.235</td>
</tr>
<tr>
<td>52</td>
<td>27.622</td>
<td>66</td>
<td>45.562</td>
<td>80</td>
<td>72.994</td>
<td>94</td>
<td>113.846</td>
<td>108</td>
<td>173.218</td>
</tr>
<tr>
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<td>47.174</td>
<td>81</td>
<td>75.413</td>
<td>95</td>
<td>117.403</td>
<td>109</td>
<td>178.330</td>
</tr>
<tr>
<td>54</td>
<td>29.724</td>
<td>68</td>
<td>48.816</td>
<td>82</td>
<td>77.904</td>
<td>96</td>
<td>121.061</td>
<td>110</td>
<td>183.571</td>
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<td>50.530</td>
<td>83</td>
<td>80.467</td>
<td>97</td>
<td>124.819</td>
<td>111</td>
<td>188.942</td>
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<tr>
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<td>70</td>
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<td>83.102</td>
<td>98</td>
<td>128.664</td>
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<td>33.149</td>
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<td>54.086</td>
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<td>57.873</td>
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<td>94.406</td>
<td>102</td>
<td>145.123</td>
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<tr>
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<td>38.232</td>
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<td>61.891</td>
<td>89</td>
<td>97.430</td>
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<td>117</td>
<td>224.107</td>
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<td>76</td>
<td>63.979</td>
<td>90</td>
<td>100.541</td>
<td>104</td>
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<td>118</td>
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<tr>
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<td>41.040</td>
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<td>66.139</td>
<td>91</td>
<td>103.738</td>
<td>105</td>
<td>158.630</td>
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<td>237.010</td>
</tr>
<tr>
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<td>42.494</td>
<td>78</td>
<td>68.357</td>
<td>92</td>
<td>107.021</td>
<td>106</td>
<td>163.368</td>
<td>120</td>
<td>243.706</td>
</tr>
</tbody>
</table>

*Tdb: °F

**P_s: lb/ft²

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2-14
1. the number of occupants,
2. the ventilation rate, and
3. the lighting and equipment loads.

In the code, these factors may have different values for each hour of occupancy.

2.8 Error Messages

Since many of the relations used in SHEP are valid only over certain ranges, limits have been placed on the values of certain input data and of certain computed variables. If these limits are exceeded, diagnostic error messages are printed, stating what variable is in error and what value it has at the time it exceeded its limit. If an input variable has an illegal value, this will be indicated and the run will terminate; if a computed variable is invalid, this fact will be printed and the run will continue. A third type of diagnostic message is generated through machine error; for instance, if an index has over-run its bound.

A list of the error messages is indicated in Table III. These error messages are incorporated into the SHEP code and are in addition to the compilation and execution diagnostic routines of the machine.

2.9 Determination of Shelter Dry-Bulb Temperature

All thermal loads and enthalpies are computed at the beginning of a time increment based upon an estimate of what the shelter dry-bulb temperature will be. Then the net amount of energy added to the shelter system during that increment is calculated. With this value, the shelter dry-bulb temperature can be computed by equation 20 of Appendix A. Since the shelter dry-bulb temperature of the increment is initially estimated to be that of the last increment, an iteration procedure is used to permit each calculated temperature
TABLE III
ERROR MESSAGES

1. Input Variables Illegal
   A. "Inclination Angle XI (___) is ___. This value must be 90° or less."
   B. "The latitude of the shelter is greater than the program can handle for this day of the year."

2. Calculated Variables Illegal
   A. "R during hour ___ is ___, which is less than 1.0. Therefore, the latent metabolic energy has been reduced."
   B. "Shelter effective temperature during hour ___ is ___, which exceeds the limits on the metabolic relations."
   C. "Shelter dry-bulb temperature during hour ___ is ___, which exceeds the limits on the metabolic relations."
   D. "The relative humidity in the shelter has exceeded saturation."

3. Procedural Errors
   A. "The limits on laymax or nmax of wall ___ have been exceeded."
   B. "The number of shelter boundaries, NW, has been exceeded."
   C. "The number of iterations for an increment has exceeded the value of IDATA(3)."
   D. "The number of increments in an hour exceeds the value of IDATA(5)."
   E. "The hour numbers are not indexing properly."
   F. "The hour number has exceeded the length of occupancy."
to be used as a new estimate to compute a more accurate shelter dry-bulb temperature.

The number of iterations for each increment is a function of the accuracy of the initial estimate. If the dry-bulb temperatures computed on two successive iterations are less than 1°F apart, the last temperature computed is assumed to be the value for the increment and the iteration procedure is curtailed. Otherwise, the procedure is continued until the number of iterations reaches the value of IDATA(3), (see Section 3).

2.10 Determination of Shelter Effective Temperature

After the shelter dry-bulb temperature for an increment has been computed, wet-bulb temperature is determined via the Carrier equation (equation 41 of Appendix A). Using a linear approximation to the nomogram of Reference 4, the effective temperature is calculated from:

\[
ET = \frac{107.5 \, T_{db} - 45.2 \, T_{wb}}{T_{db} - T_{wb} + 62.3} \quad \text{for} \quad \begin{cases} 
45^\circ F \leq T_{db} \leq 110^\circ F \\
30^\circ F \leq T_{wb} \leq 110^\circ F
\end{cases}
\]

where

- \( T_{db} \) = dry-bulb temperature, °F
- \( T_{wb} \) = wet-bulb temperature, °F

The psychrometric condition of the shelter atmosphere at the beginning of the next increment is then set equal to that at the end of the last increment and calculations for the next increment are begun. When one hour's calculations have been completed, the values for the last increment of the hour are printed out as the conditions at the end of the hour.
SECTION 3

INPUT DATA

Input data consist of physical constants, hourly occupancy constants, geometrical and thermal characteristics of the shelter, and initial conditions. The input variables and their definitions are given below; where units are not indicated, the value is dimensionless.

ALAT - Latitude of the shelter, degrees. The limits on the range of ALAT are a function of the time of the year, see Figure 3-1.

ALONG - Longitude of the shelter, degrees. Only values in the range 0° to 180° W are allowed.

ALT - Altitude of the shelter, feet.

AREA(j) - Area of boundary j, ft².

ASOIL(j) - Control constant determining the media exterior to the outer surface of boundary j.

\[ \text{ASOIL}(j) = \begin{cases} 
-1 & \text{ambient air} \\
0 & \text{interior air} \\
1 & \text{soil}
\end{cases} \]

AZ(j) - Azimuth angle of boundary j. AZ(j) is measured in a clockwise direction from north to the outward-pointing normal to the boundary. Values between 0° and 360° are permitted. For a boundary facing east, AZ(j) = 90°; if it faces west, AZ(j) = 270°.

BF - Cooling coil bypass factor of the air conditioning unit. It is defined as

\[ BF = \frac{t_f - t_e}{t_d - t_e} \]

where

\[ t_f = \text{air temperature leaving the coil, °F} \]

\[ t_e = \text{coil effective surface temperature, °F (TCOIL)} \]

\[ t_d = \text{air temperature entering the coil, °F} \]

The suggested value is 0.15.
Figure 3-1 Allowable Values of the Shelter Latitude, AIAT

Latitude of shelter must remain below this curve during the occupancy period.
CFMIN - Total ventilation rate through air conditioner, cfm.

CON(k,j) - Thermal conductivity of material of layer k of boundary j, Btu/hr-ft°F.

CP(k,j) - Specific heat of material of layer k of boundary j, Btu/lb°F.

D - Day number of the start of occupancy. Values in the range of 1-365 are allowed, e.g., for January 1, D = 1.

DP(k,j) - Thickness of layer k of boundary j, feet.

DT - Time increment of shelter history used in finite-difference equations, hrs. 0.00 < DT ≤ 0.500 hours, DT = 0.167 is suggested.

DX(k,j) - Nodal point spacing of layer k of boundary j, feet.

EQTIM(i) - Equation of Time for day i, hours. See Table I.

F1 - Total ventilation rate entering shelter, cfm.

F2 - Total ventilation rate of outside air entering shelter system, cfm.

GG - Equivalent interior length of shelter, feet. Equivalent dimensions are those of a parallelepiped approximating the shelter under analysis.

HH - Equivalent interior height of shelter, feet.

HI(j) - Interior film heat transfer coefficient of boundary j, Btu/hr-ft°F.

HO(j) - Exterior film heat transfer coefficient of boundary j, Btu/hr-ft²°F.

HRS - Total number of continuous hours of shelter occupancy.

IDATA(1) - Sets initial boundary temperatures

\[ IDATA(1) = \begin{cases} 1 & \text{all boundary nodes have different temperatures} \\ 0 & \text{all boundary nodes have same temperature} \end{cases} \]

IDATA(2) - Reference constant; IDATA(2) = 0 is suggested.

IDATA(3) - Number of iterations for computing incremental shelter dry-bulb temperature. IDATA(3) = 4 is suggested.

IDATA(4) - Number of shelters to be analyzed in the computer run.
IDATA(5) -1 hour/DT, rounded to the nearest integer.

IDATA(6) -Sets type of boundary.

\[
\begin{align*}
\text{IDATA(6)} &= \begin{cases} 
1 & \text{for all non-adiabatic boundaries} \\
0 & \text{for all adiabatic boundaries}
\end{cases}
\end{align*}
\]

IDATA(7) -Determines presence of air conditioning.

\[
\begin{align*}
\text{IDATA(7)} &= \begin{cases} 
0 & \text{no air conditioning} \\
1 & \text{air conditioning is present}
\end{cases}
\end{align*}
\]

IDATA(8) -Reference constant, IDATA(8) = 0 is suggested.

IDATA(9) -Reference constant, IDATA(9) = 0 is suggested.

IDATA(10) -Sets atmospheric condition for solar radiation.

\[
\begin{align*}
\text{IDATA(10)} &= \begin{cases} 
0 & \text{for clear atmosphere} \\
1 & \text{for industrial atmosphere}
\end{cases}
\end{align*}
\]

IDATA(11) -Establishes format of printout.

\[
\begin{align*}
\text{IDATA(11)} &= \begin{cases} 
1 & \text{Standard output format} \\
0 & \text{Only maximum, minimum and average temperatures are printed}
\end{cases}
\end{align*}
\]

IDATA(12) -Establishes variability of occupancy values.

\[
\begin{align*}
\text{IDATA(12)} &= \begin{cases} 
0 & \text{P, Fl, CFMIN, QLITE, QEQUIP change for each hour.} \\
1 & \text{These variables are held constant for entire occupancy.}
\end{cases}
\end{align*}
\]

IDATA(13) -Establishes variability of inlet values.

\[
\begin{align*}
\text{IDATA(13)} &= \begin{cases} 
1 & \text{Inlet conditions held constant for entire occupancy} \\
0 & \text{These variables change for every hour of occupancy.}
\end{cases}
\end{align*}
\]

INT(m) -Hour limits of the intervals for which average temperatures are desired, e.g., for average dry-bulb temperatures from hour number 3 to hour number 9 of occupancy, then INT(1) = 3, INT(2) = 9. INT(m), where m is an odd integer, 1 ≤ m ≤ 59 determines the start of an interval; and INT(m+1) determines the end of the interval.

LAYMAX(j) -Number of layers in boundary j. Soil back of a boundary or an air space within a boundary is considered a layer of the boundary. Value must be 5 or less.

LST(1) -Local Standard Time at beginning of occupancy; defined in terms of military time (0-23 hrs).

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3-4
NMAX(j) - Number of nodal points in boundary j. If a boundary is soil-backed, the nodal points extend into and through the soil, up to a suggested distance of 10 feet. Integral values up to 39 are permitted. The outermost nodal point is not included in this value.

NOINT - Number of time intervals for which average temperatures are desired, NOINT ≤ 30.

NW - Number of boundaries in the shelter, NW ≤ 20.

P - Number of occupants.

PSAT(n) - Saturation pressure of water vapor at n °F, lb/ft^2. See Table II.

QEQUIP - Sensible heat load due to mechanical and/or electrical equipment (excluding lighting), Btu/hr.

QLITE - Sensible heat load due to lighting, Btu/hr.

ROW(k,j) - Density of material of layer k of boundary j, lb/ft^3.

R11 - Relative humidity of inlet air at beginning of occupancy.

R12 - Relative humidity of inlet air at end of each hour of occupancy.

R2 - Relative humidity in shelter at beginning of occupancy.

TA1 - Dry-bulb temperature of air exterior to shelter structure at beginning of occupancy, °F.

TA2 - Dry-bulb temperature of air exterior to shelter structure at end of each hour of occupancy, °F.

TCOIL - Effective coil temperature of air conditioning unit, °F. Suggested value is 55°F with WCOIL = 0.00921 lb water/lb dry air.

TD11 - Dry-bulb temperature of inlet air at the beginning of occupancy, °F.

TD12 - Dry-bulb temperature of inlet air at end of each hour of occupancy, °F.

TD2 - Initial shelter dry-bulb temperature, °F.

TEFF(l) - Initial shelter effective temperature, °F.

TO - Initial temperature of each boundary nodal point, °F.

TRANS(j) - Total radiation transmittance of boundary j.

TSOIL(j) - Temperature of outermost nodal point when considering a soil-backed boundary j, °F.
TWB(1) - Initial shelter wet-bulb temperature, °F.

W - Equivalent interior width of shelter, feet.

WCOIL - Humidity ratio at saturation corresponding to TCOIL, lb moisture/lb dry air. Suggested value is 0.00921 for TCOIL = 55°F.

XI(j) - Inclination angle of boundary j, measured from the vertical, degrees. Values between 0° and 90° are allowed. For a vertical boundary, XI(j) = 0°.

Limitations on Input Values

Since relations exist between certain inputs, changing one necessitates adjusting related values. These related input values are:

1. If the time increment DT is varied, adjust IDATA(5), since IDATA(5) = 1 hour/DT, rounded to the nearest integer.
2. For the NW boundaries, the boundary properties of AREA(j), ASOIL(j), AZ(j), HI(j), HO(j), LAYMAX(j), NMAX(j) must correspond.
3. If the number of layers, LAYMAX(j), is changed, then layer properties must be added or deleted: CON, CP, DP, DX, ROW.
4. Equivalent dimensions GG, HH, W must correspond to the AREA(j) values.
5. The hour limits on the interval for which average temperatures are desired, INT(m), must not exceed the length of occupancy, HRS.
6. The values of \[ \sum_j (DP(j)/DX(j)) + 1 \] must equal NMAX for each boundary.
7. Initial values of dry-bulb, wet-bulb, and effective temperature and relative humidity must correspond: TD2, TWB(1), TEFF(1), R2.
8. WCOIL must correspond to TCOIL, for the air conditioning unit.

It is obvious that the size of the data deck is quite large; it is of utmost importance that the order of the data deck, as indicated in Figure 3-2, be maintained. Decimal points and field widths of the variables are also
* Note: The sequence of input cards 5-6-7-8 is repeated for each boundary in succession; i.e., for J from 1 to NW.

+ Note: Input card 6 is included in the sequence for boundary J only if ASOIL(J) < 0.0.

Figure 3-2 Input Data Format

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3-7
* See Note on preceding page.

++ Note: Input card 7 is included in the sequence only if ASOIL(J) < 0.0 and XI(J) < 90.0.

** Note: Input card 8 is repeated for each layer of boundary J, i.e., for K from 1 to LAYMAX(J) for boundary J.

* Note: Input card 10 is included only for those boundaries for which ASOIL(J) > 0.0.

" Note: Input card 11 is included once if IDATA(1) = 0. If IDATA(1) = 1, card 11 must be repeated for each nodal point of each boundary, in succession; i.e., for K from 1 to LAYMAX(J) for each J from 1 to NW.

Figure 3-2 (Cont'd) Input Data Format
* Note: Input card 13 is included only if NOINT > 0, and is repeated for each lower and upper hour number for each interval in succession; i.e., for I from 1 to 2 * (NOINT).
++ Note: Input card 15 is included only if IDATA(12) < 0, and is repeated for each hour of occupancy after the first; i.e., for hour numbers from 2 to HRS.
+++ Note: Input card 16 is included only if IDATA(13) < 0, and is repeated for each hour of occupancy after the first; i.e., for hour numbers from 2 to HRS.
indicated in the figure. Since data may be placed only in specific fields on each data card, the easiest method of keeping the data deck ordered is to punch an appropriate identifier anywhere outside of the specified fields.

Values for the matrices EQTIM and PSAT may be found in Tables I and II. The EQTIM values are those for the year 1958, and may be considered those for any year in this century. Values of the saturation pressure as a function of dry-bulb temperature are introduced as a table with a linear interpolation scheme included in the program. These two inputs comprise the first 436 cards of a standard data deck.

If the program is used to analyze an actual shelter under actual weather conditions, hourly ambient temperature and relative humidity values are required. Soil temperatures may be considered constant over a two-week occupancy period.

Various time increments (DT) were tested by the authors to determine a compromise between accuracy of computation and length of computation. It has been found that a time increment of ten minutes (0.167 hr) produces results which are, on the average, within 0.3°F of the results calculated using 2-minute increments. The computation time is also decreased by approximately 60%, see Figure 3-3.

It should be noted that integer data values must be right-hand justified within their respective fields; if this is not the case, the machine will place zeroes in the field to the right of the right-most non-zero digit.
Figure 3-3  Shelter Effective Temperature Computed on Three Different Time Increments
SECTION 4

HOW TO USE SHEP

4.1 The first step in the analysis of a shelter is to describe the shelter with all of its necessary characteristics. Answer these questions on a form sheet such as that of Figure 4-1.

1. Where is the shelter located? (ALT, ALAT, ALONG).
2. What is the shelter geometry? How many separate "walls"? (NW, GG, HH, W).
3. How many occupants will be in the shelter and will this number change during the period of occupancy? (P).
4. What is the total ventilation airflow entering shelter and will it change with time? (Fl).
5. What is the lighting and equipment load and is it constant? (QLITE, QEQUIP).
6. How long is the period of occupancy and when does it start (day of the year and time of day)? (D, HRS, LST(1)).
7. For each boundary, what are the values of the:
   A. Area? (AREA).
   B. Number of layers and number of nodal points? (LAYMAX, NMAX).
   C. Interior and exterior film heat transfer coefficients? (HI, HO).
   D. Control number for the wall backing? (ASOIL).
   F. Inclination and azimuth angles? (XI, AZ).
8. For each layer of each boundary, what are the values of the:
   A. Thickness? (DP).
   B. Nodal Point Space? (DX).
Figure 4-1 Form Sheet for Organizing Input Data
For each boundary:

<table>
<thead>
<tr>
<th>Boundary No.</th>
<th>AREA</th>
<th>LAYMAX</th>
<th>NMAX</th>
<th>HI</th>
<th>HO</th>
<th>ASOIL</th>
<th>TRANS</th>
<th>XI</th>
<th>AZ</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td></td>
<td></td>
<td></td>
<td></td>
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</table>

Figure 4-1 (Cont’d) Form Sheet for Organizing Input Data
For each layer of each boundary: DP(t/h), DX(f/h), CON(Btu/hr-fl*-F), ROW(lb/ft²), CP(Btu/lb*-F)

<table>
<thead>
<tr>
<th>Layer</th>
<th>Boundary 1</th>
<th>Boundary 2</th>
<th>Boundary 3</th>
<th>Boundary 4</th>
<th>Boundary 5</th>
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<tr>
<td></td>
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<td>3</td>
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</tr>
</tbody>
</table>

Figure 4-1 (Cont'd) Form Sheet for Organizing Input Data
9 AIR CONDITIONING: CFMIN \[\text{cfm}\], TCOIL \[\text{°F}\], WCOIL \[\text{lb moisture/lb dry air}\], BF \[\text{cyl}\], F2 \[\text{cyl}\], CFMAX \[\text{cfm}\].

INITIAL CONDITIONS: TD2 \[\text{°F}\], R2 \[\text{deg}\], TWB(I) \[\text{°F}\], TEFF(I) \[\text{°F}\].

10 SOIL TEMPERATURES:

<table>
<thead>
<tr>
<th>Boundary No.</th>
<th>Temperature</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td></td>
</tr>
<tr>
<td>2</td>
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</tr>
<tr>
<td>4</td>
<td></td>
</tr>
<tr>
<td>5</td>
<td></td>
</tr>
</tbody>
</table>

11 INITIAL NODAL-POINT TEMPERATURES: TO \[\text{°F}\] or Individual Values

| Nodal-Point | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 |
|-------------|---|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|

12 TIME INCREMENT: DT \[0.1\] hr

13 INTERVAL LIMITS: \[.1\] TO \[.1\]

Figure 4-1 (Cont'd) Form Sheet for Organizing Input Data.
14

INITIAL INLET CONDITION: TA1 °F, TA2 °F, TDII °F, TD12 °F, RI1 °F, R12 °F

15-16

For each hour of occupancy:

<table>
<thead>
<tr>
<th>Hour No.</th>
<th>TA2</th>
<th>TD12</th>
<th>RI2</th>
<th>P</th>
<th>F1</th>
<th>CFMIN</th>
<th>QLITE</th>
<th>QEQUIP</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
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<td></td>
<td></td>
</tr>
</tbody>
</table>

Figure 4-1 (Cont'd) Form Sheet for Organizing Input Data
C. Thermal Conductivity? (CON).

D. Density? (ROW).

E. Specific Heat? (CP).

9. If air conditioning is involved, what air flow is going through the cooler (CFMIN); what is the effective surface coil temperature (TCOIL) and the humidity ratio corresponding to this dewpoint temperature (WCOIL); what is the bypass factor (BF)? What is the amount of outside air entering the system (F2)?

10. What are the initial conditions inside the shelter? (TD2, R2, TWB(l), TEFF(l)). What are the initial wall temperatures? (TO).

11. What are the soil temperatures around the shelter? (TSOIL).

12. For computational purposes:

   A. How many intervals are there for which average temperatures are required, and what are their hour limits? (NOINT, INT).

   B. What time increment should shelter temperatures be calculated on? (DT).

13. What are the hourly values of inlet temperature and relative humidity during occupancy? (TA2, TD12, R2). What are the values of occupancy variables (P, Fl, CFMIN, QLITE, QEQUIP)?

4.2 After the data is determined, options in the program must be decided upon. Will the analysis include:

   1. Initially isothermal boundaries? (IDATA(1)).

   2. Adiabatic or non-adiabatic boundaries? (IDATA(6)).

   3. Air conditioning? (IDATA(7)).

   4. Printout of the table of hourly values? (DATA(11)).
5. Constant or time-varying occupancy variables? (IDATA(12)).
6. Constant or time-varying inlet conditions? (IDATA(13)).

4.3 Once the data has been determined and the options have been chosen, initial conditions in the shelter system must be set. Four quantities must be given to specify the shelter atmosphere: dry-bulb, wet-bulb and effective temperatures, and the relative humidity. It is mandatory that these values correspond to each other.

Initial wall temperatures should approximate the initial shelter dry-bulb temperature within a few degrees. While stability of solution is not a problem in the code, initial conditions should be fairly accurate so that the number of calculations required to eliminate the errors introduced by the incorrect estimate of the shelter and boundary temperatures is minimized.

4.4 After all values necessary for an analysis have been determined, the code user is ready to create the data deck. The format of each data card and the order of the cards is indicated in Figure 3-2. Of course, the order of the deck is of major importance and an identification on each data card will help keep it in its correct position.

4.5 The SHEP code is written in FORTRAN IV specifically for the CDC 3600 computer system and, therefore, utilizes certain library functions. These include:

<table>
<thead>
<tr>
<th>Form</th>
<th>Definition</th>
</tr>
</thead>
<tbody>
<tr>
<td>ABSF(X)</td>
<td>Absolute value of X</td>
</tr>
<tr>
<td>ATAN(X)</td>
<td>Arctangent X radians</td>
</tr>
<tr>
<td>COS(X)</td>
<td>Cosine X radians</td>
</tr>
<tr>
<td>EXP(X), EXPF(X)</td>
<td>e to the $x^{th}$ power</td>
</tr>
<tr>
<td>SIN(X)</td>
<td>Sine X radians</td>
</tr>
<tr>
<td>SQRT(X)</td>
<td>Square root of X</td>
</tr>
<tr>
<td>TANF(X)</td>
<td>Tangent X radians</td>
</tr>
</tbody>
</table>
If the code is re-written for another computer system, these library functions, or their equivalents, must be supplied.

4.6 If the values of certain input data and certain computed variables exceed specified ranges, error messages will appear in the output as per Table III, p. 2-16.

The SHEP code requires two memory banks \((65^k\) locations) for the code and the accompanying matrices; in fact, the AINV matrix, which contains the inverted matrices of the temperature coefficients in the boundary heat-transfer equations, fills one bank \((76,400\) out of \(77,777\) (octal) words). Thus, a BANK statement is another requirement. There are only two computer systems other than the 3600 that have this amount of storage known to the authors at the time of this writing; they are the CDC 6600 and the UNIVAC 1108. Although several smaller computers can be adapted and enlarged, this requires special facilities. Therefore, in terms of storage requirements, the SHEP code can be run on any of these three computing systems.
SECTION 5

INTERPRETATION OF OUTPUT

The output of the SHEP program is a tabulation of the instantaneous values of the thermal loads affecting the shelter and the shelter psychrometric condition for the last increment of each hour of occupancy, see Figure 5-1. It must be remembered that these values are instantaneous and, while they reflect trends in the shelter system, interpolation between hourly values may be invalid. Also, hourly thermal loads determine the resultant shelter temperature, not vice versa. The 3600 computer system printer includes a procedure for rounding output to the format specified. Thus, the thermal loads are rounded in value to the nearest integer.

The air conditioning, boundary and condensation heat loads, when positive, represent energy lost from the shelter system; all other positive loads are energy additions. In the SHEP code, the assumptions associated with the calculations of the air conditioning, moisture condensation, and transmitted solar radiation loads generally lead to conservative estimates of these loads.

Maximum and minimum shelter temperatures and the hours of their occurrence are indicated. Average temperatures are computed for the entire occupancy period, for each full day of occupancy, and for specific intervals determined by the code user.
### Figure 5-1: Typical Output of SHEP Code

<table>
<thead>
<tr>
<th>Day</th>
<th>Min.</th>
<th>Max.</th>
<th>Average</th>
<th>Median</th>
<th>3rd</th>
<th>1st</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>72.2</td>
<td>72.6</td>
<td>72.4</td>
<td>72.4</td>
<td>72.1</td>
<td>72.2</td>
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<td>71.8</td>
<td>71.8</td>
<td>71.6</td>
<td>71.6</td>
</tr>
</tbody>
</table>

**Notes:**
- The table represents time-averaged temperature values for each day of occupancy.
- Values are for specific intervals.
- The table details minimum, maximum, and average temperature data for each day.

---

**Temperature Data:**
- Min. Temp.: 71.2°F
- Max. Temp.: 72.6°F
- Average Temp.: 72.4°F

---

**Energy Consumption:**
- Trans. Metabolic: 74.2 Btu/hr
- Sensible: 72.8 Btu/hr
- Lighting: 72.0 Btu/hr
- Equipment: 70.4 Btu/hr

---

**Other Details:**
- Normal Occupant Activity Level: 40.0 BTU/HR
- Effective Duration of Occupancy: 15 hours
- Hot Water Temperature: 120°F
- Supply Air Temperature: 68°F
- Ventilation Air Change Rate: 0.5 Air Changes per Hour
SECTION 6
SAMPLE PROBLEM

To illustrate the use of the SHEP code, a shelter defined by the values listed in Table IV is considered. A sketch of the sample shelter is shown in Figure 601; the rectangular shelter area is in the basement of a multi-story building. It is defined by eight opaque boundaries, four of which are multi-layered; three are soil-backed, two boundaries are exposed to ambient air, and the remaining three are exposed to interior spaces. See Figures 2-1 and 2-2. Occupancy is limited to 1000 persons for 24 hours at a constant ventilation rate of 15 cfm/occupant. The air conditioning system is assumed to be operating during occupancy with a constant airflow rate of 8 cfm-occupant and the shelter lighting and equipment add a constant thermal load of 11,250 Btu/hr. The weather affecting the shelter is that which occurred at Montgomery, Alabama during 1 August, 1963.

The output of this shelter analysis is shown in Figure 501. It can be seen that the shelter temperatures vary in a diurnal cycle, as would be expected; they are lowest in the early morning and are highest in the late afternoon. Air conditioning also can be seen to vary directly with the shelter temperature. In the cooler hours of the day, i.e., from 10 PM to 9 AM, the shelter boundaries are warmer than the shelter atmosphere, and energy is transferred from the boundaries to the shelter air, as is indicated by the negative signs on the boundary heat losses for these hours. During the other hours of the day, the shelter is warmer than the boundaries and energy leaves the shelter.

If the value of condensation heat loss is negative, this corresponds to evaporation of the condensate on the walls, and an addition of energy to
### TABLE IV
SAMPLE INPUT DATA

<table>
<thead>
<tr>
<th></th>
<th>EQTIM(1)</th>
<th>EQTIM(365)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>PSAT(50)</td>
<td>PSAT(120)</td>
</tr>
<tr>
<td>3</td>
<td>DATA(I−13)</td>
<td></td>
</tr>
<tr>
<td>4</td>
<td>LOCATION: ALT 2100 ft, ALAT 86.4°N, ALONG 32.3°W</td>
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</tr>
<tr>
<td></td>
<td>GEOMETRY: NW 8, GG 75.0 ft, HH 100 ft, W 1340 ft</td>
<td></td>
</tr>
<tr>
<td></td>
<td>OCCUPANTS: P 1000</td>
<td></td>
</tr>
<tr>
<td></td>
<td>TOTAL VENTILATION: FI 15000 cfm</td>
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<tr>
<td></td>
<td>LIGHTING and EQUIPMENT: QLITE 6250 Btu/hr, QEQUIP 5000 Btu/hr</td>
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<td>OCCUPANCY PERIOD: D 213, HRS 24 hours, LST(I) 0, NOINT 4 intervals</td>
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</table>
### TABLE IV (Cont'd)

**SAMPLE INPUT DATA**

<table>
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<th>Boundary No.</th>
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<th>LAYMAX</th>
<th>NMAX</th>
<th>HI</th>
<th>HO</th>
<th>ASOIL</th>
<th>TRANS</th>
<th>XI</th>
<th>AZ</th>
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### TABLE IV (Cont'd)

**SAMPLE INPUT DATA**

For each layer of each boundary: DP(f1), DX(f1), CON(Btu/hr-ft-F), ROW(lb/ft²), CP(Btu/lb-F)

<table>
<thead>
<tr>
<th>Layer</th>
<th>Boundary 1</th>
<th>Boundary 2</th>
<th>Boundary 3</th>
<th>Boundary 4</th>
<th>Boundary 5</th>
<th>Boundary 6</th>
<th>Boundary 7</th>
<th>Boundary 8</th>
<th>Boundary 9</th>
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<th>Boundary 20</th>
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<tr>
<td>DP</td>
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</tbody>
</table>
TABLE IV (Cont'd)
SAMPLE INPUT DATA

9  AIR CONDITIONING: CFMIN 8000.00 cfm, TCOIL 55.0°F, WCOIL 0.00921 lb moisture/lb dry air, BF 30.18°F, F2 3000.00 cfm

INITIAL CONDITIONS: TD2 58.1°F, R2 0.476, TWB(1) 75.8°F, TEFF(1) 79.0°F

10  SOIL TEMPERATURES:

<table>
<thead>
<tr>
<th>Boundary No.</th>
<th>Temperature</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>75.0</td>
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<td>2</td>
<td>75.0</td>
</tr>
<tr>
<td>3</td>
<td>75.0</td>
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</tbody>
</table>

11  INITIAL NODAL-POINT TEMPERATURES: TO 81.8°F or Individual Values

12  TIME INCREMENT: DT 0.167 hr

13  INTERVAL LIMITS:

<table>
<thead>
<tr>
<th>Boundary No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
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<tr>
<td>4</td>
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Nodal-Point

<table>
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</table>
TABLE IV (Cont'd)
SAMPLE INPUT DATA

14 INITIAL INLET CONDITION: TAI 75.0°F, TA2 75.0°F, TDII 75.0°F, TD12 75.0°F, RII 0.0, RI2 0.0

15-16 For each hour of occupancy:

<table>
<thead>
<tr>
<th>Hour No.</th>
<th>TA2</th>
<th>TDI2</th>
<th>RI2</th>
<th>P</th>
<th>FI</th>
<th>CFMIN</th>
<th>QLITE</th>
<th>QEQUIP</th>
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</tbody>
</table>
Figure 6-1 Sketch of Shelter Area Used in Sample Problem
the shelter temperature. Positive value of the condensation heat load indicates moisture is condensing on the shelter boundaries and energy is being removed from the shelter air. There is a check in the code to prevent the amount of re-evaporated moisture from exceeding the amount previously condensed.

Metabolic loads are predicted, using the relations developed by Houghten (5), based on both the shelter dry-bulb and effective temperatures. Since these vary by only a few degrees during occupancy, the total metabolic load for each hour is approximately constant.
REFERENCES


APPENDICES
The study of the interrelationships among ventilation rate, thermal load, and boundary losses in the shelter is based on the assumption that the shelter atmosphere may be represented by one psychrometric condition. A shelter model that will take into account the thermal effects of solar radiation, air-conditioning, moisture condensation and re-evaporation, and boundary losses is developed according to the following assumptions:

1) the air within the shelter is completely and instantaneously mixed;
2) the film heat transfer coefficients are constant for any one boundary surface;
3) the radiative energy transfer within the shelter can be neglected;
4) the condition of the air exhausted from the shelter is the condition of the shelter atmosphere;
5) the thermal and physical properties of the structural materials and of air are not temperature-dependent;
6) the incident solar radiation is absorbed on the outer surface of the boundaries and appears as conducted energy or is transmitted into the shelter and is considered an instantaneous load with the lighting and equipment loads; and
7) the thermal loads and the psychrometric states of the inlet and exhaust air are constant over short time intervals.

The shelter model is therefore a volume enclosed by boundaries into which sensible and latent heat loads and ventilating air are introduced and from which air is exhausted and energy is lost, see Figure A-1. The governing equations of the enclosed volume are derived from the conservation of mass and the conservation of energy.
Air Conditioning → Inlet → Air → Exhaust Air

Temperature

Shelter Enthalpy

Metabolic

Transmitted Solar

Moisture Condensation

Lighting

Equipment

Boundary Losses

Figure A-1 Shelter Energy Transfer
\[
\frac{\partial}{\partial t} (H) + \frac{\partial}{\partial t} (H_S) + \frac{\partial}{\partial t} (Q_M + Q_L + Q_E) - \frac{\partial}{\partial t} (Q_W + Q_{AC}) = 0 \quad (1)
\]

where
\[H = \text{enthalpy of the exchanged air, Btu}\]
\[H_S = \text{enthalpy of the shelter, Btu}\]
\[Q_M = \text{metabolic energy of occupants, Btu}\]
\[Q_L = \text{energy due to shelter lighting, Btu}\]
\[Q_E = \text{energy due to other shelter equipment, Btu}\]
\[Q_W = \text{energy conducted through shelter boundaries, Btu}\]
\[Q_{AC} = \text{energy removed from shelter system by air conditioner, Btu}\]

Integrating equation (1) over the time increment \(\delta t\) yields

\[
(H_1 - H_2) + (H_{S,1} - H_{S,2}) + Q_M + Q_L + Q_E - Q_W - Q_{AC} = C \quad (2)
\]

where the subscripts 1 and 2 refer to the beginning and the end of the time increment, respectively. Although this analysis is time-varying in the sense that results using successive time increments represent changing conditions, by assumption (7), the thermal load values and the psychrometric states of the inlet and exhaust air in this equation are all considered constant during the time increment. Therefore, there is no heat-storage term during the time increment and \(C = 0\).

Conservation of mass may be applied to both the dry air and the water vapor in the shelter system. When it is applied to the vapor:

\[
\frac{\partial}{\partial t} (M_V) + \frac{\partial}{\partial t} (M_{V,S}) + \frac{\partial}{\partial t} (M_{V,M}) - \frac{\partial}{\partial t} (M_{V,COND}) = 0 \quad (3)
\]

where
\[M_V = \text{mass of water vapor in the exchanged air, lb.}\]
\[M_{V,M} = \text{mass of water vapor introduced by the shelter occupants, lb.}\]
\[M_{V,S} = \text{mass of water vapor in the shelter air, lb.}\]
\[M_{V,COND} = \text{mass of water vapor removed by condensation, lb.}\]

Integration yields

\[
(M_{V,1} - M_{V,2}) + (M_{V,S,1} - M_{V,S,2}) + M_{V,M} - M_{V,COND} = 0 \quad (4)
\]

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A-3
The energy balance for dry air in the system is given by

\[
\frac{\partial}{\partial t} (M_a) + \frac{\partial}{\partial t} (M_{a,s}) = 0
\]  

(5)

where \( M_a \) = mass of dry air in the exchanged air, lb.

\( M_{a,s} \) = mass of dry air in the shelter air, lb.

or

\[
(M_a,1 - M_{a,2}) + (M_{a,s,1} - M_{a,s,2}) = 0
\]

(6)

Let

\[
\delta Q = H_1 + H_{S1} + Q_M + Q_L + Q_E - Q_W - Q_{AC}
\]

(7)

\[
M_{V,0} = M_{V,1} + M_{V,S,1} + M_{V,M} + M_{V,COND}
\]

(8)

\[
M_{a,0} = M_{a,1} + M_{a,s,1}
\]

(9)

then

\[
\delta Q = H_2 + H_{S,2}
\]

(10)

\[
M_{V,0} = M_{V,2} + M_{V,S,2}
\]

(11)

\[
M_{a,0} = M_{a,2} + M_{a,s,2}
\]

(12)

Now

\[
H_{S,2} = M_{a,s,2} h_{a,s,2} + M_{V,S,2} h_{V,S,2}
\]

(13)

and

\[
H_2 = M_{a,2} h_{a,2} + M_{V,2} h_{V,2}
\]

(14)

where the lower case h's refer to specific enthalpies (Btu/lb).

Since the ventilating air leaves at the shelter condition,

\[
h_{a,2} = h_{a,s,2}
\]

(15)

and

\[
h_{V,2} = h_{V,S,2}
\]

(16)

Substituting this value for the incremental energy \( \delta Q \):

\[
\delta Q = M_{a,0} h_{a,s,2} + M_{V,0} h_{V,S,2}
\]

(17)
Now specific enthalpies of dry air and water vapor may be given as functions of dry-bulb temperature:

\[ h_a = 0.24 \, T_{db} \]  \hspace{1cm} (18)

and

\[ h_v = 1061.0 + 0.444 \, (T_{db}) \]  \hspace{1cm} (19)

Combining equations (17) through (19) and solving for the dry-bulb temperature leads to

\[ T_{db} = \frac{\delta Q - 1061 \, M_{V,0}}{0.444 \, M_{V,0} + 0.24 \, M_{a,0}} \]  \hspace{1cm} (20)

This represents the shelter dry-bulb temperature at the end of the time increment \( \delta T \).

Expressions for \( M_{a,0} \) and \( M_{V,0} \) can be found, since

\[ M_{a,2} = 60 \, \dot{F}_2 \, \rho_{a,2} \, \delta \tau \]  \hspace{1cm} (21)

\[ M_{V,2} = 60 \, \dot{F}_2 \, \rho_{V,2} \, \delta \tau \]  \hspace{1cm} (22)

\[ M_{a,s,2} = V \rho_{a,s,2} \]  \hspace{1cm} (23)

and

\[ M_{V,s,2} = V \rho_{V,s,2} \]  \hspace{1cm} (24)

where

\[ V = \text{shelter volume, ft}^3 \]

\[ \rho_{a,2} = \text{density of dry air leaving shelter, lb/ft}^3 \]

\[ \rho_{V,2} = \text{density of water vapor leaving shelter, lb/ft}^3 \]

\[ \rho_{a,s,2} = \text{density of dry air in shelter, lb/ft}^3 \]

\[ \rho_{V,s,2} = \text{density of water vapor in shelter, lb/ft}^3 \]

and \( \dot{F}_2 \) = mass flow rate of exhaust air, lb/hr.
We have assumed that

\[ \rho_{a,2} = \rho_{a,s,2} \]  \hspace{1cm} (25)

and \[ \rho_{v,2} = \rho_{v,s,2} \]  \hspace{1cm} (26)

Therefore, we obtain the expression:

\[ M_{V,0} = \rho_{v,2} (60 \dot{F}_2 \delta \tau + V) \]  \hspace{1cm} (27)

and \[ M_{a,0} = \rho_{a,2} (60 \dot{F}_2 \delta \tau + V) \]  \hspace{1cm} (28)

Now, when these equations are solved for the ventilation rate \( \dot{F}_2 \),

\[ \dot{F}_2 = \frac{M_{a,0} - \rho_{a,2} V}{60 \delta \tau \rho_{a,2}} = \frac{M_{V,0} - \rho_{v,2} V}{60 \delta \tau \rho_{v,2}} \]  \hspace{1cm} (29)

It is assumed that the densities of dry air and of water vapor may be determined from the perfect-gas law: Therefore,

\[ \rho_v = \frac{P_v}{R_v (T_{db} + 459.69)} \]  \hspace{1cm} (30)

and

\[ \rho_a = \frac{P_b - P_v}{R_a (T_{db} + 459.69)} \]  \hspace{1cm} (31)

where \( P_b \) = barometric pressure, \( lb/ft^2 \)

\( P_v \) = partial pressure of water vapor, \( lb/ft^2 \)

\( R_v \) = gas constant for water vapor, \( ft-lb/lb\ mole \cdot °R \)

and \( R_a \) = gas constant for dry-air, \( ft-lb/lb\ mole \cdot °R \)

with \( P_b = (9.8 \times 10^{-7}) A^2 - 0.0759 A + 2116.2 \) \hspace{1cm} (32)

where \( A \) = altitude, ft.

Now, the partial pressure of water vapor is expressible as

\[ P_v = r P_s \]  \hspace{1cm} (33)

where \( r \) = relative humidity in the shelter

and \( P_s \) = saturation pressure of water vapor, \( lb/ft^2 \)
Saturation pressure varies with dry-bulb temperature according to

\[ P_s = 5.132 \exp (0.0329 T_{db}) \]  \hspace{1cm} (34)

Using the values

\[ R_a = 53.35 \text{ ft-lb/lb mole - } ^\circ R \]
\[ R_v = 85.71 \text{ ft-lb/lb mole - } ^\circ R \]

leads to

\[ P_v = r \left( 5.132 \exp (0.0329 T_{db}) \right) \]  \hspace{1cm} (35)

\[ \rho_v = \frac{r}{(T_{db} + 459.69)} \left( 0.05987 \exp (0.0329 T_{db}) \right) \]  \hspace{1cm} (36)

and \[ \rho_a = \frac{1}{T_{db} + 459.69} \left[ 1.84 \times 10^{-8} + 0.00142A + 35.68 - r(0.0962 \exp(0.0329 T_{db}) \right] \]  \hspace{1cm} (37)

Since \[ \frac{M_{a,o}}{\rho_{a,2}} = \frac{M_{v,o}}{\rho_{v,2}} \]  \hspace{1cm} (37)

from equations (27) and (28), we can evaluate the last three equations to obtain

\[ P_v = \frac{P_b}{1 + 0.6224 \left( \frac{M_{a,o}}{M_{v,o}} \right)} \]  \hspace{1cm} (39)

Relative humidity, as given by equation (33), becomes

\[ r = \frac{P_b}{(5.132 e(0.0329 T_{db})) (1 + 0.6224 \left( \frac{M_{a,o}}{M_{v,o}} \right))} \]  \hspace{1cm} (40)

To summarize, the two equations necessary to compute the shelter condition are (20) and (40). The quantities in these equations may be computed as outlined above. Although the dry-bulb temperature and relative humidity uniquely determine the condition of the shelter air,
it is desired to express this condition in terms of dry-bulb temperature and wet-bulb temperature.

The wet-bulb temperature can be determined using the Carrier equation:

\[ P_v = P_s' - \left( \frac{P_b - P_s'}{2800.0 - 1.3 T_{wb}} \right) \]  \hspace{1cm} (41)

where \( P_s' \) = saturation pressure at wet-bulb temperature, lb/ft\(^2\)

\( T_{wb} \) = wet-bulb temperature, °F

\( P_s' \) may be evaluated from equation (34) as

\[ P_s' = 5.132 \exp(0.0329 T_{wb}) \]  \hspace{1cm} (42)

\( P_v \) is obtained from equation (39). Equation (41) is then a transcendental equation in \( T_{wb} \) and may be solved by an iteration procedure. After both the dry-bulb and wet-bulb temperatures are known, the effective temperature may then be calculated from

\[ ET = \frac{107.5 T_{db} - 45.2 T_{wb}}{62.3 + T_{db} - T_{wb}} \]  \hspace{1cm} for \( 45°F \leq T_{db} \leq 110°F \)  \hspace{1cm} (43)

\[ 30°F \leq T_{wb} \leq 100°F \]
APPENDIX B

DETERMINATION OF SOLAR RADIATION INTENSITY

B-1  Determination of the Sun's Altitude and Azimuth Angles

Consider an earth-centered right-handed rectilinear coordinate system with the Y-axis directed toward the sun and with the X-Y plane that of the equator, see Figure B-1. The unit normal vectors \( \hat{i}, \hat{j}, \) and \( \hat{k} \) are parallel to the X, Y and Z axes, respectively. The rays of the sun are parallel to the unit vector \( \hat{s} \). The unit vector \( \hat{n} \) at a point on the surface of the earth \( P \) is normal to the position vector of \( P \) and oriented toward the north pole. The position vector is parallel to the unit vector \( \hat{r} \). The point \( P \) is located on the surface of the earth by the hour angle, \( \theta \), and the latitude angle, \( \phi \).

Now
\[
\begin{align*}
\hat{r} &= \cos \phi \sin \theta \hat{i} - \cos \phi \cos \theta \hat{j} + \sin \phi \hat{k} \quad (1) \\
\hat{s} &= \cos \eta \hat{j} + \sin \eta \hat{k} \quad (2)
\end{align*}
\]

where: \( \eta \) = declination angle of the sun.

The sun's zenith angle, \( \psi \), is given by
\[
\psi = \arccos (\hat{r} \cdot \hat{s})
= \arccos \left( \sin \phi \sin \eta - \cos \phi \cos \theta \cos \eta \right) \quad (3)
\]

The sun's altitude angle, \( \beta \), is
\[
\beta = \frac{\pi}{2} - \psi \quad (4)
\]

Thus
\[
\beta = \arcsin \left( \sin \phi \sin \eta - \cos \phi \cos \theta \cos \eta \right) \quad (5)
\]

Now the vector \( \hat{n} \) is
\[
\hat{n} = -\sin \phi \sin \theta \hat{i} + \sin \phi \cos \theta \hat{j} + \cos \phi \hat{k} \quad (6)
\]

Taking \( \hat{n} \cdot \hat{s} \), since \( \hat{n} \cdot \hat{r} = 0 \), gives
\[
\hat{n} \cdot \hat{s} = \sin \phi \cos \theta \cos \eta + \cos \phi \sin \eta \quad (7)
\]
horizontal plane on earth's surface at P

ray from sun

projection of sun's rays on horizontal plane parallel to ray from sun

equator of earth

where:

\[ \beta = \text{altitude angle of sun} \]

\[ \psi = \text{zenith angle of sun} \]

\[ \gamma = \text{azimuth angle of sun} \]

\[ \theta = \text{hour angle} \]

Figure B-1 Geometry for Solar Radiation
Also \( \hat{n} \cdot \hat{s} = \cos T \cos \beta \) \( (8) \)

where: \( T = \) sun's azimuth angle.

Therefore,

\[ T = \arccos \left[ \frac{\sec \beta (\cos \phi \sin \eta + \sin \phi \cos \theta \cos \eta)}{1 + \sin \phi \cos \eta} \right] \] \( (9) \)

Thus the sun's altitude and azimuth angles are determined as a function of latitude, \( \phi \), solar declination angle, \( \eta \), and time angle, \( \theta \).

B-2 Solar Declination Angle and Time Angle

The solar declination angle, \( \eta \), is given as a function of the day of the year, see Figure B-2. This variation was approximated by the following function, namely,

\[ \eta = 0.410 \sin \left[ \frac{\pi}{122.5} (D-80) \right] \] \( (10) \)

where: \( D = \) day of the year, 1 to 365.

The time angle, \( \theta \), is denoted by

\[ \theta = \frac{\pi}{12} (T_{\text{solar}}) \] \( (11) \)

where

\( T_{\text{solar}} = \) solar time, hrs, see Section 2.2.

B-3 Angle of Surface to Sun's Rays

Consider a tilted plane surface at an angle, \( \xi \), to a vertical surface at a point \( P \) on the surface of the earth, see Figure B-3. The unit normal to the tilted surface, \( \hat{n}_s \), is at the angle \( \xi \) to the normal to the vertical surface which makes an angle, \( T - a \), with respect to the projection of the sun's rays on a horizontal surface at point \( P \). If a right-handed rectilinear coordinate system is defined at point \( P \), such that the \( X \)-axis is parallel to the direction of the projection of the sun's ray, \( \hat{s} \), on the horizontal plane and the \( Y \)-axis is parallel to the vertical plane, the \( X \)-\( Z \) plane is the horizontal plane. Let the unit
Figure B-2 Variation of Declination Angle, $\eta$, with the Day of the Year
Figure B-3 Geometry for Tilted Surfaces
vectors $\hat{i}$, $\hat{j}$ and $\hat{k}$ be directed along the $X$, $Y$ and $Z$ axes, respectively. Then the unit normal to the tilted surface, $\hat{n}_s$, is

$$\hat{n}_s = \cos(T-a) \cos \xi \hat{i} + \sin \xi \sin(T-a) \cos \xi \hat{j} + \sin(T-a) \cos \xi \hat{k}$$  \hspace{1cm} (12)

where: $a =$ azimuth of the normal to the vertical surface measured westward from north

$T =$ azimuth of sun measured westward from north

Then

$$\hat{s} \cdot \hat{n}_s = \cos \beta \cos(T-a) \cos \xi + \sin \beta \sin \xi$$  \hspace{1cm} (13)

but $\hat{s} \cdot \hat{n}_s = \cos \alpha$  \hspace{1cm} (14)

where:

$\alpha =$ angle between the normal to the tilted surface and the sun's rays

Therefore

$$\alpha = \arccos (\cos \beta \cos(T-a) \cos \xi + \sin \beta \sin \xi)$$  \hspace{1cm} (15)

B-4 Sunrise and Sunset Values of Hour Angle

At sunrise, $\beta = 0$; then from equation (5) have

$$0 = \arcsin (\sin \phi \sin \eta - \cos \phi \cos \theta_r \cos \eta)$$

or $\theta_r = \arccos (\tan \phi \tan \eta)$  \hspace{1cm} (16)

where: $\theta_r =$ value of $\theta$ at sunrise

However, the relation

$$-1 \leq \tan \phi \tan \eta \leq 1$$

must hold.
Now the calculation of solar radiation is restricted to the northern hemisphere:

\[ 0 \leq \phi \leq \frac{\pi}{2} \]  

(17)

and, from Figure B-2, \( \eta \) varies as

\[-0.410 \leq \eta \leq 0.410 \]  

(18)

Thus, to satisfy the restriction on the \( \phi \) and \( \eta \) values, the ranges must be

\[ \phi + \eta \leq \frac{\pi}{2} \]  

(19)

and \[ \phi \leq \frac{\pi}{2} \]  

(20)

Since \( \eta \) is a function of the day of the year, these restrictions indicated that there is a maximum value of latitude, \( \Phi \), that can be considered at each day of the year, see Figure 3-1.

The value of the hour angle for sunset, \( \Theta_s \), is

\[ \Theta_s = 2\pi - \Theta_r \]  

(21)

Thus, for \( \Theta_r \leq \Theta \leq \Theta_s \) there can be some form of solar radiation upon a surface as long as \( 0 \leq \beta \leq \frac{\pi}{2} \).

B-5 Intensity of Solar Radiation

The intensity of solar radiation that will be incident upon a surface is given by

\[ I = I_{\text{DIR}} + I_{\text{DIF}} + I_{\text{REF}} \]  

(22)

where:

- \( I_{\text{DIR}} \) = intensity of direct solar radiation
- \( I_{\text{DIF}} \) = intensity of diffuse solar radiation
- \( I_{\text{REF}} \) = intensity of solar radiation reflected from the ground and surrounding surfaces onto the surface
The assumption is made that the reflected solar radiation from the surroundings is negligible, \( I_{REF} = 0 \).

Thus

\[
I = I_{DIR} + I_{DIF}
\]

(23)

The direct solar radiation is given by

\[
I_{DIR} = \begin{cases} 
I_{DN} \cos \alpha & 0 \leq \alpha \leq \pi/2 \\
0 & \alpha > \pi/2
\end{cases}
\]

(24)

where: \( I_{DN} \) = intensity of direct normal solar radiation; i.e., the direct radiation on a surface normal to the sun's rays.

The intensity of the direct normal solar radiation, \( I_{DN} \), is given as a function of the sun's altitude angle, \( \beta \), (from Reference 6), see Figure B-4. The data are approximated by the relationships

\[
I_{DN} = \begin{cases} 
294 \left(1 - e^{-\frac{10}{\pi} \beta}\right) & \text{for clear air} \\
200 \left(1 - e^{-\frac{7}{\pi} \beta}\right) & \text{for industrial air}
\end{cases}
\]

(25)

for \( \beta > 0 \).

The intensity of the diffuse solar radiation is assumed to be defined by

\[
I_{DIF} = I_{DIF,V} + (I_{DIF,H} - I_{DIF,V}) \sin \xi
\]

(26)

where: \( I_{DIF,V} \) = intensity of diffuse solar radiation on a vertical surface

\( I_{DIF,H} \) = intensity of diffuse solar radiation on a horizontal surface.

The ratio of the intensity of diffuse solar radiation on a vertical surface to the intensity of diffuse solar radiation on a horizontal surface is given as a function of the cosine of the angle between the normal to the vertical surface and the sun's rays (from Reference 7), see Figure B-5.
Figure B-4  Direct Normal Radiation as a Function of $\beta$

\[ I_{DN} = 294(1 - e^{-\frac{10}{\pi}\beta}) \]

\[ I_{DN} = 200(1 - e^{-\frac{7}{\pi}\beta}) \]

SOLAR ALTITUDE ANGLE, $\beta$
Figure B-5  Ratio of Diffuse Sky Radiation Incident Upon a Vertical Surface to that Incident Upon a Horizontal Surface During Clear Days (Ref. 7)
The results are approximated by

\[
\frac{I_{\text{DIF},Y}}{I_{\text{DIF},H}} = \begin{cases} 
0.44 & \text{for } \cos \beta \cos (T-a) \leq -0.4 \\
0.625 [\cos \beta \cos (T-a)]^2 + 0.525 \cos \beta \cos (T-a) + 0.55 & \text{for } -0.4 < \cos \beta \cos (T-a) < 0 \\
0.35 [\cos \beta \cos (T-a)]^2 + 0.45 \cos \beta \cos (T-a) + 0.55 & \text{for } \cos \beta \cos (T-a) \geq 0 
\end{cases} \tag{27}
\]

Then

\[
I_{\text{DIF}} = I_{\text{DIF},H} \left[ (1 - \sin \xi) f(\beta, T-a) + \sin \xi \right] \tag{28}
\]

The ratio of the total intensity of solar radiation, \(I_{\text{TH}}\), on a horizontal surface to the intensity of diffuse solar radiation on a horizontal surface, \(I_{\text{DIF},H}\), is given as a function of the direct normal solar radiation intensity (from Reference 8), see Figure B-6. The relationship can be approximated by

\[
\frac{I_{\text{TH}}}{I_{\text{DIF},H}} = 0.667 \times 10^{-6} (I_{\text{DN}})^3 - 1.5 \times 10^{-4} (I_{\text{DN}})^2 + 0.0183 (I_{\text{DN}}) + 1 \tag{29}
\]

It may be assumed that

\[
I_{\text{TH}} = I_{\text{DIR},H} + I_{\text{DIF},H} = I_{\text{DN}} \sin \beta + I_{\text{DIF},H} \tag{30}
\]

Therefore,

\[
I_{\text{DIF},H} = \frac{I_{\text{DN}} \sin \beta}{I_{\text{TH}}/I_{\text{DIF},H} - 1} \tag{31}
\]

Combining equation (31) and equation (28) gives

\[
I_{\text{DIF}} = \frac{\sin \beta [f(\beta, T-a) (1 - \sin \xi) + \sin \xi]}{0.667 \times 10^{-6} (I_{\text{DN}})^3 - 1.5 \times 10^{-4} (I_{\text{DN}})^2 + 0.0183} \tag{32}
\]

with total radiation on a surface given by equation (23).
Figure B-6  Ratio of Total to Diffuse Solar Radiation on a Horizontal Surface
vs Direct Normal Radiation, $I_{DN}$ (Ref. 8)
Heat transfer by conduction through the shelter boundaries is determined by the temperature of each boundary inner surface. To calculate these temperatures, the temperature profile through each boundary is determined by the solution of a set of implicit finite-difference equations. Since each boundary may be multi-layered (up to 5 layers), the nodal point coefficients must be determined individually for each layer.

For this solution, a layer is divided into slabs $\delta x$ thick. A temperature nodal point is assigned to the node of each slab; for the interior slabs, this point is at the midpoint of each slab, and for the innermost and outermost slabs, there is another point at the surface of the slab. If the boundary under analysis is multi-layered, a similar nodal point array accompanies each layer.

Nodal point temperatures are determined by the appropriate heat transfer equation at each nodal point. There are four basic heat balances that can occur at a node; the one to be used depends on the position of the node in question. These four positions are (1) at the inner surface of the boundary; (2) in the interior of any layer of the boundary; (3) at an interface between layers of the boundary; and (4) at the exterior surface of the boundary, see Figure C-1.

Position 1 - at the inner surface of a boundary. The heat transfer in this case is by convection with the shelter air and by conduction.
Figure C-1 Various Positions of Boundary Nodal Points
with the next slab in the layer. Heat transfer due to moisture condensation may also be present, see Appendix D. The general heat balance for deriving the various nodal point temperature equations is

\[
\begin{bmatrix}
\text{energy entering slab } n \\
\text{from preceding slab (n-1)}
\end{bmatrix} - \begin{bmatrix}
\text{energy leaving slab } n \\
to succeeding slab (n+1)
\end{bmatrix} = \text{energy stored in slab } n
\]

For position 1, the equation becomes:

\[
q_{\text{condensation}} + q_{\text{convection}} - q_{\text{conduction}} = q_{\text{stored}}
\]

or

\[
C + h_1 (T_{db,s} - T_n) - \frac{k}{\delta x} (T_n - T_{n+1}) = \frac{C_p \delta x}{2 \delta T} (T_n - T_n')
\]

where

- \( C \) = condensation term, see Appendix D.
- \( h_1 \) = interior film heat-transfer coefficient, Btu/hr-ft\(^2\)-°F
- \( T_{db,s} \) = dry-bulb temperature of shelter, °F
- \( T_n \) = temperature of node \( n \), °F
- \( k \) = thermal conductivity of layer material, Btu/hr-ft-°F
- \( \delta x \) = thickness of slab in layer, ft.
- \( T_{n+1} \) = temperature of node \( (n+1) \), °F
- \( \rho \) = density of layer material, lb/ft\(^3\)
- \( C_p \) = specific heat of layer material, Btu/lb
- \( \delta T \) = time increment, hr.
- \( T_n' \) = temperature of node \( n \) in preceding time increment, °F.

The matrix solution of simultaneous equations requires that the coefficients of the nodal temperatures are dimensionless. Therefore, the transformed energy balance for the inner surface nodal point is

\[
(1.0 + \frac{k}{h_1 \delta x} + \frac{\rho C_p \delta x}{2 h_1 \delta T}) T_n - (\frac{k}{h \delta x}) T_{n+1} = \frac{\rho C_p \delta x}{2 h_1 \delta T} T_n
\]

\[
+ T_{db,s} + \frac{C}{h_1}
\]

\[
(3)
\]
which in matrix element notation is
\[ a_{m} T_{n} + a_{n,n+1} T_{n+1} = b_{n} \] (4)
or, since the inner surface nodal point is indexed 1,
\[ a_{11} T_{1} + a_{12} T_{2} = b_{1} \] (5)

**Position 2** - in the interior of any layer of the boundary. In this case, conduction into and out of slab \( n \) is the only heat transfer. Therefore, the energy balance becomes
\[ \frac{k}{\delta x} (T_{n-1} - T_{n}) - \frac{k}{\delta x} (T_{n} - T_{n+1}) = \frac{\rho c_{p} \delta x}{\delta T} (T_{n} - T_{n}') \] (6)
where \( T_{n-1} \) = temperature of node \((n - 1)\), °F
This becomes, in dimensionless quantities,
\[ -T_{n-1} + \left( \frac{(\delta x)^2 \rho c_{p}}{k \delta T} + 2 \right) T_{n} - T_{n+1} = \frac{\rho c_{p} (\delta x)^2}{k \delta T} T_{n} \] (7)
which is of the form
\[ a_{n} T_{n-1} + a_{n,n} T_{n} + a_{n,n+1} T_{n+1} = b_{n} \] (8)

**Position 3** - at an interface between layers \((m, \text{ and } (m+1))\) of a boundary. Again, the only heat transfer is conduction, but since the successive layers will have different thermal properties, the energy balance is:
\[ \frac{k_{m}}{\delta x_{m}} (T_{n-1} - T_{n}) - \frac{k_{m+1}}{\delta x_{m+1}} (T_{n} - T_{n+1}) = \frac{\rho_{m} c_{p,m} \delta x_{m}}{2 (\delta x_{m})} \]
\[ + \frac{\rho_{m+1} c_{p,m+1} \delta x_{m+1}}{2 (\delta x_{m+1})} (\frac{T_{n} - T_{n}'}{\delta T}) \] (9)
or, in dimensionless form,
\[ -T_{n-1} + \left( 1 + \frac{k_{m+1} \delta x_{m}}{k_{m} \delta x_{m+1}} \right) + \frac{\rho_{m+1} c_{p,m+1} \delta x_{m+1}}{2 k_{m} \delta T} + \frac{\rho_{m+1} c_{p,m+1} \delta x_{m+1}}{2 k_{m} \delta T} T_{n} \]
\[ + \left( \frac{k_{m+1} \delta x_{m}}{k_{m} \delta x_{m+1}} \right) T_{n+1} = \left( \frac{\rho_{m} c_{p,m} \delta x_{m}^2 + \rho_{m+1} c_{p,m+1} \delta x_{m+1} \delta x_{m} \delta x_{m+1}}{2 k_{m} \delta T} \right) T_{n}' \] (10)
which is of the form:

\[ a_{n,n-1} T_{n-1} + a_{n,n} T_n + a_{n,n+1} T_{n+1} = b_n \]  

(11)

Position 4 - at the exterior surface of the boundary. This case has several variations, depending on whether the external surface boundary is exposed to either soil or air.

If the boundary is backed by soil, the only mode of heat transfer will be conduction. The only difference between position 4 and position 2 is that the unknown temperatures \( T_{n+1} \) in equation (7) is replaced by the known temperature of the soil, \( T_{\text{soil}} \), and this term, being known, becomes part of the \( b \) coefficient:

\[ T_{n-1} + \left( \frac{\rho c_p (\delta x)^2}{k \delta T} + 2 \right) T_n = \frac{\rho c_p (\delta x)^2}{k \delta T} T_{n-1} + T_{\text{soil}} \]  

(12)

If the backing of the wall is ambient air, convection enters as well as solar radiation. The energy balance is

\[ \frac{k}{\delta x} (T_{n-1} - T_n) + q_{\text{solar}} - h_o (T_n - T_a) = \frac{\rho c_p \delta x}{2 \delta T} (T_n - T_n') \]  

(13)

where \( q_{\text{solar}} \) = solar radiation load on boundary, Btu/hr.

\( h_o \) = exterior film heat transfer coefficient, Btu/hr-ft\(^2\)-\(^\circ F\)

\( T_a \) = dry-bulb temperature of ambient air, \( ^\circ F \)

In dimensionless form,

\[ \left( -\frac{k}{h_o \delta x} \right) T_{n-1} + \left[ \frac{k}{h_o \delta x} + 1 + \frac{\rho c_p \delta x}{h_o \delta T} \right] T_n = \frac{q_{\text{solar}}}{h_o} + T_a + \frac{\rho c_p \delta x}{257 h_o} T_n' \]  

(14)

Both equations (12) and (14) are of the form

\[ a_{n,n-1} T_{n-1} + a_{n,n} T_n = b_n \]  

(15)
If the wall is backed by interior air, \( q_{\text{solar}} = 0 \), and \( T_a \) is the average of the shelter temperature and the ambient temperature.

After all coefficients of all nodal points in a boundary have been evaluated, the equations are solved simultaneously using a Gauss-Jordan method of matrix inversion. Convection transfer through a boundary is then computed as

\[
q_b = h_i (T_{db,s} - T_1)
\]

where \( T_1 \) = temperature of the inner surface nodal point and the total boundary heat loss is

\[
q_b = \sum_{\text{walls}} q_b
\]
The process of moisture condensing on, or re-evaporating from, a surface involves both a mass and an energy transfer. The analysis used in this study parallels that of Jakob\(^{(9)}\).

The following differential equations may be set up for moving fluids, relating thermal conduction and mechanical diffusion:

\[
\frac{\partial T}{\partial t} + \nu \frac{\partial T}{\partial x} + \nu \frac{\partial T}{\partial y} + \nu \frac{\partial T}{\partial z} = \alpha \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) \tag{1}
\]

and

\[
\frac{\partial p}{\partial t} + \nu \frac{\partial p}{\partial x} + \nu \frac{\partial p}{\partial y} + \nu \frac{\partial p}{\partial z} = \delta \left( \frac{\partial^2 p}{\partial x^2} + \frac{\partial^2 p}{\partial y^2} + \frac{\partial^2 p}{\partial z^2} \right) \tag{2}
\]

where  
\( T = \) absolute temperature, °F  
\( v = \) velocity, ft/hr  
\( p = \) partial pressure of water vapor, lb/ft\(^2\)  
\( \alpha = \) thermal diffusivity, ft\(^2\)/hr  
\( \delta = \) mechanical diffusivity, ft\(^2\)/hr

Newton's Law yields

\[
q'' = -k \frac{dt}{dn} \tag{3}
\]

and Fick's Law gives

\[
m'' = \delta \frac{dc}{dn} \tag{4}
\]

where  
\( q'' = \) rate of heat flow per unit area, Btu/ft\(^2\)-hr  
\( m'' = \) rate of mass flow per unit area, lb/ft\(^2\)-hr  
\( n = \) direction of heat and mass flow, ft  
\( k = \) thermal conductivity of the medium, Btu/hr-ft-°F  
\( c = \) concentration, lb/ft\(^3\)
Define \[ m = m_v + m_a \] where \( m_v \) = mass of water vapor in shelter volume, lb
\( m_a \) = mass of dry air in shelter volume, lb

Define \[ \rho = \frac{m}{V} = \frac{m_v}{V} + \frac{m_a}{V} = \rho_v + \rho_a \] where \( \rho \) = density, lb/ft\(^3\)
\( V \) = volume of shelter, ft\(^3\)

Define \[ W = \frac{m_v}{m_a} \]

Define \( c_v \) = concentration of vapor in dry air (assumed to) = \( \rho_v \)
\( c_a \) = concentration of dry air in water vapor (assumed to) = \( \rho_a \)

Now, from (4)
\[ \dot{m}_v = -\delta \frac{dc_v}{dn} = -\delta \frac{d\rho_v}{dn} = -\delta \frac{m_v}{V} \frac{d(V)}{dn} \]
\[ = -\delta \frac{m_a}{V} \frac{d(m_a)}{dn} = -\delta(\frac{m_a}{V}) \frac{dW}{dn} \]
\[ \dot{m}_v = -\delta \rho_a \frac{dW}{dn} \] (8)

From (3) \[ \Delta x_T \int_0^\Delta x_T \frac{dW}{dn} = \int_T^{T_s} k dT \] (9)

where \( \Delta x_T \) = thermal boundary layer thickness, ft.
\( T_o \) = temperature of the environment, °R
\( T_s \) = temperature of the boundary surface, °R

which leads to \[ q = \frac{k}{\Delta x_T} (T_o - T_s) \] (10)

Similarly, equation (8) leads to \[ \dot{m}_v = \frac{\delta \rho_a}{\Delta x_w} (W_o - W_s) \] (11)
where $\Delta x_w = \text{mechanical boundary layer thickness, ft.}$

$W_o = \text{humidity ratio of shelter environment, lb_w/lb_a}$

and $W_s = \text{humidity ratio at boundary temperature, lb_w/lb_a}$

Parallel expression to equations (10) and (11) are

$q = h (T_o - T_s)$  \hspace{1cm} (12)

and $\dot{m}_v = \rho a b (W_o - W_s)$  \hspace{1cm} (13)

where $b = a \text{ coefficient of mass transfer, which must be evaluated.}$

A comparison of equation (10) with (12), and (11) with (13) shows

$h = \frac{k}{\Delta x_T}$  \hspace{1cm} (14)

and $b = \frac{\delta}{\Delta x_w}$  \hspace{1cm} (15)

It is assumed that the thermal and mechanical boundary layer thickness are very nearly equal:

$\Delta x_T = \Delta x_w$  \hspace{1cm} (16)

Therefore: $\frac{h}{b} = \frac{k}{\delta}$  \hspace{1cm} (17)

or $\frac{h}{\rho a c p b} = \frac{k}{\rho a c p \delta} = \frac{\alpha}{\delta}$  \hspace{1cm} (18)

where $\alpha = \text{thermal diffusivity} = \frac{k}{\rho a c p}$

Therefore, $b = \frac{h}{\rho a c p} \left(\frac{\delta}{\alpha}\right)$  \hspace{1cm} (19)

Now, for water diffusing into air, $\frac{\alpha}{\delta} = 0.917$ (Ref. 9)

since $\alpha = 0.070 \text{ ft}^2/\text{hr}$ for air

and $\delta = 0.765$ for water vapor at $0^\circ \text{C}$ and 760 mm Hg.
Therefore
\[ b = \frac{h}{\rho_a c_p} \left( \frac{1}{0.917} \right) \]
\[ = 1.09 \left( \frac{h}{\rho_a c_p} \right) \]
and
\[ \dot{m}_v = \rho_a b (W_o - W_s) \]
\[ = 1.09 \left( \frac{h}{\rho_a c_p} \right) (W_o - W_s) \]
where
\[ c_p = \text{specific heat of air-water vapor mixture} \]
\[ \approx 0.24 \text{ Btu/lb}^\circ\text{F} \]

Since
\[ q = \dot{m}_v \lambda \]
where
\[ \lambda = \text{heat of condensation, Btu/lb} \]
\[ q_{\text{condensation}} = \frac{1.09h}{\rho_a c_p} (W_o - W_s) \]

Now, since
\[ W = 0.622 \frac{p'}{p_b - p'} \]
where
\[ W = \text{humidity ratio} \]
\[ p' = \text{partial pressure of water vapor,} \]
\[ p_b = \text{barometric pressure,} \]
we may approximate
\[ W_o - W_s = 0.622 \left( \frac{p_o}{p_b - p_o} - \frac{p_s}{p_b - p_s} \right) \]

Therefore the heat transfer due to condensation is expressible by:
\[ q_{\text{condensation}} = 2.825 \frac{\lambda h}{\rho_a} \left( \frac{p_o}{p_b - p_o} - \frac{p_s}{p_b - p_s} \right) \]
and condensation is determined to be present if \( p_o > p_s \). This is the condensation term of equations (1) and (2) of Appendix C. Also, equation (26) expresses the heat transfer due to re-evaporation of the condensate, if the energy and mass transfer phenomena are assumed to be equivalent.
in the two processes. In the case of evaporation, \( p_s > p_o \) and the
q_{\text{condensation}} term is negative (\( C < 0 \)). The value of \( \rho_a \) in equation (26)
is assumed to be defined by

\[
\rho_a = 3.25 \times 10^{-7} T^2 - 1.86 \times 10^{-4} T + 0.0863
\]  

(27)

where \( T \) = the average of the temperature of the boundary surface
in question and the shelter dry-bulb temperature, °F.
APPENDIX E

ERROR INTRODUCED BY CONSIDERING THREE-DIMENSIONAL HEAT TRANSFER AS A ONE-DIMENSIONAL PHENOMENON

If a shelter boundary is curved, such as in a tunnel, the one-dimensional heat transfer calculations introduce errors because the heat flow is no longer one-dimensional. But the one-dimensional analysis is applicable to such situations. A comparison of the relative rates of heat transfer will determine the error of the application.

For a flat boundary, the heat transmitted from the inner surface to nodal point n is

\[ q = -kA \frac{T_1 - T_n}{\Delta x} \]  

(1)

where

- \( k \) = thermal conductivity of flat surface along a normal, \( \text{Btu/hr-ft}^2\text{OF} \)
- \( A \) = area of the boundary, \( \text{ft}^2 \)
- \( T_1 \) = temperature of inner surface of boundary, \( \text{OF} \)
- \( T_n \) = temperature of nth nodal point, \( \text{OF} \)
- \( \Delta x \) = distance along a normal between nodal points i and n, \( \text{ft} \).

Heat transfer through a spherical layer of the boundary from the inner surface of the boundary to nodal point n is:

\[ q = -k(\frac{4\pi r^2}{r}) \frac{dT}{dr} \]  

(2)

which, for steady state, may be integrated to

\[ q = k(\frac{4\pi}{r_n}) T_{\frac{1}{r_1} - \frac{1}{r_n}} \]  

(3)
where \( r_1 \) = radius of curvature of the inner surface of the boundary

\( r_n \) = radius of curvature to the nth nodal point

See Figure E-1.

This is equivalent to

\[ q = \frac{1}{\beta} k A_m \frac{T_1 - T_n}{\Delta r} \]

(4)

where \( A_m \) = heat conductance area at the average radius

\[ A_m = 4\pi \frac{(r_1 + r_n)^2}{2} \]

and

\[ \beta = \frac{1}{2} + \frac{1}{4} \left( \frac{r_1}{r_n} \right) + \frac{1}{4} \left( \frac{r_n}{r_1} \right) \]

(6)

\( \beta \) represents the difference in calculating heat transfer using the two analyses; it represents the percent departure of the one-dimensional analysis from the three-dimensional analysis. Values of \( \beta \) as a function of \( \frac{r_n}{r_1} \) are shown in Table V.

Using a similar analysis for cylindrical coordinates, the expression for \( \beta \) becomes

\[ \beta = \frac{1}{2} \left( \frac{r_n}{r_1} \right) \ln \left( \frac{r_n}{r_1} \right) \]

(7)

and its variation with \( \left( \frac{r_n}{r_1} \right) \) is also given in Table V.

Now say a tunnel with a radius of ten feet were used as a shelter. Assume, too, that the boundary is soil-backed and therefore the maximum outermost nodal point is ten feet past the outer surface of the boundary.
Figure E-1  Nodal Point Radii in a Cylindrical Shelter  
Used in Determining the $\beta$ Error
TABLE V

ERRORS OF CONSIDERING THREE-DIMENSIONAL HEAT TRANSFER AS ONE-DIMENSIONAL

<table>
<thead>
<tr>
<th>( \frac{r_n}{r_1} )</th>
<th>( \beta ) (Cylindrical)</th>
<th>( \beta ) (Spherical)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.0</td>
<td>1.0</td>
<td>1.0</td>
</tr>
<tr>
<td>1.1</td>
<td>1.001</td>
<td>1.002</td>
</tr>
<tr>
<td>1.2</td>
<td>1.003</td>
<td>1.008</td>
</tr>
<tr>
<td>1.3</td>
<td>1.006</td>
<td>1.017</td>
</tr>
<tr>
<td>1.4</td>
<td>1.010</td>
<td>1.029</td>
</tr>
<tr>
<td>1.5</td>
<td>1.014</td>
<td>1.042</td>
</tr>
<tr>
<td>1.6</td>
<td>1.018</td>
<td>1.056</td>
</tr>
<tr>
<td>1.7</td>
<td>1.023</td>
<td>1.072</td>
</tr>
<tr>
<td>1.8</td>
<td>1.029</td>
<td>1.089</td>
</tr>
<tr>
<td>1.9</td>
<td>1.034</td>
<td>1.107</td>
</tr>
<tr>
<td>2.0</td>
<td>1.040</td>
<td>1.125</td>
</tr>
<tr>
<td>2.1</td>
<td>1.046</td>
<td>1.144</td>
</tr>
<tr>
<td>2.2</td>
<td>1.051</td>
<td>1.164</td>
</tr>
<tr>
<td>2.3</td>
<td>1.057</td>
<td>1.184</td>
</tr>
<tr>
<td>2.4</td>
<td>1.063</td>
<td>1.204</td>
</tr>
<tr>
<td>2.5</td>
<td>1.068</td>
<td>1.225</td>
</tr>
</tbody>
</table>
Therefore,

\[
\frac{r_n}{r_1} = \frac{r_1 + \Delta p + 10}{r_1} = 2 + \frac{\Delta p}{10}
\]  

(8)

where \( p \) is the thickness of the boundary. A reasonable value of \( p \) would be 3 feet and thus the error in the heat flow due to using a one-dimensional analysis method of a three-dimensional analysis is 5.7% using the cylindrical surface analysis or 18.4% using the spherical surface analysis. (See Table V.) Generally, a tunnel designed as a mass shelter can be expected to have a radius greater than ten feet; therefore, the error introduced would be correspondingly less. Hence a shelter boundary that is curvilinear can be treated as a flat surface with an error given by equation (6) or (7).
APPENDIX F

ESTIMATION OF ERROR ASSOCIATED WITH CALCULATION OF AIR-CONDITIONING LOAD

The performance of an air-conditioning system is a function of the environmental conditions, the psychrometric state of the air entering the unit, the performance characteristics of the components comprising the system, the flow field in the unit and the characteristics of the heat sink and source reservoirs. Procedures are required to define an air-conditioning system for primarily cooling the air introduced into the shelter. The operating principles for such a unit can be based upon a large number of choices. However, in almost every choice, a coil will be utilized for cooling and dehumidifying the air. Therefore, the SHEEP code has been constructed so as to require only the specification of the coil. It is assumed that once the coil has been defined, the designer can develop a system to produce the specified coil performance.

In particular, the coil is specified by denoting

1) a coil bypass factor,
2) an effective coil surface temperature, and
3) an air flow rate across the coil.

It is known that the coil bypass factor and effective coil surface temperature are a function of the thermal load, i.e., the psychrometric state and flow rate of the air through the coil. In the SHEEP code, this load dependence is neglected (since performance is a function of the design of the entire system) and the bypass factor and effective coil surface temperature are assumed constant.*

*This procedure is a generalization of a coil selection procedure presented in "Fundamentals of Psychrometrics - Part II", T200-20, Carrier Air Conditioning Company, page 18.

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F-1
The accuracy of this procedure has been checked by comparison with the performance data of an actual air-conditioning unit, see Table VI. It was found that neither the deduced bypass factor nor the deduced effective coil surface temperature are constant. However, if median values of the range of each of these parameters are used to calculate the capacity of the unit, this calculated unit capacity differs from the actual unit capacity by at most 37% and generally by less than 12%. This agreement is considered sufficient for the inclusion of this simplified specification for the air-conditioning equipment in the SHEP code.
TABLE VI

ESTIMATION OF ERROR ASSOCIATED WITH CALCULATION OF AIR CONDITIONING LOAD*

<table>
<thead>
<tr>
<th>Air Temperatures at Evaporator</th>
<th>Deduced Effective Coil Surface Temperature (°F)</th>
<th>Deduced Bypass Factor</th>
<th>Evaporator Air Flow (cfm)</th>
<th>Actual Unit Capacity (Btu/hr)</th>
<th>Calculated Unit Capacity (Btu/hr)</th>
<th>% Error in Calculated Unit Capacity</th>
</tr>
</thead>
<tbody>
<tr>
<td>Entering Dry-Bulb (°F)</td>
<td>Entering Wet-Bulb (°F)</td>
<td>Leaving Dry-Bulb (°F)</td>
<td>Leaving Wet-Bulb (°F)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>113.1</td>
<td>82.2</td>
<td>72.5</td>
<td>66.6</td>
<td>60.7</td>
<td>0.227</td>
<td>630</td>
</tr>
<tr>
<td>112.6</td>
<td>77.8</td>
<td>66.3</td>
<td>60.3</td>
<td>54.1</td>
<td>0.214</td>
<td>605</td>
</tr>
<tr>
<td>102.1</td>
<td>83.1</td>
<td>70.9</td>
<td>66.4</td>
<td>54.1</td>
<td>0.347</td>
<td>637</td>
</tr>
<tr>
<td>102.1</td>
<td>78.0</td>
<td>64.6</td>
<td>59.3</td>
<td>47.5</td>
<td>0.179</td>
<td>602</td>
</tr>
<tr>
<td>102.3</td>
<td>72.1</td>
<td>59.0</td>
<td>54.1</td>
<td>48.7</td>
<td>0.190</td>
<td>602</td>
</tr>
<tr>
<td>92.3</td>
<td>73.6</td>
<td>58.0</td>
<td>54.0</td>
<td>39.5</td>
<td>0.345</td>
<td>605</td>
</tr>
<tr>
<td>91.8</td>
<td>66.6</td>
<td>51.7</td>
<td>47.4</td>
<td>43.3</td>
<td>0.156</td>
<td>605</td>
</tr>
</tbody>
</table>


**Unit capacity calculated by the use of a constant bypass factor of 0.252 (median of deduced extreme values) and a constant effective coil surface temperature of 50°F (median of deduced extreme values).
APPENDIX G
TYPICAL THERMAL PROPERTIES AND DENSITIES OF BUILDING MATERIALS, SOILS, ETC.

**BUILDING MATERIAL**

<table>
<thead>
<tr>
<th>BUILDING MATERIAL</th>
<th>Thermal Conductivity CON (Btu/hr-ft-°F)</th>
<th>Specific Heat CP (Btu/lb-°F)</th>
<th>Density ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>I Building Board</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Asbestos-cement Board</td>
<td>0.33</td>
<td>0.270</td>
<td>120.00</td>
</tr>
<tr>
<td>2. Gypsum or Plastic Board ( \frac{3}{8} )&quot;</td>
<td>0.10</td>
<td>0.270</td>
<td>50.00</td>
</tr>
<tr>
<td>&quot; &quot; &quot; ( \frac{1}{2} )&quot;</td>
<td>0.09</td>
<td>0.270</td>
<td>50.00</td>
</tr>
<tr>
<td>3. Plywood</td>
<td>0.07</td>
<td>0.500</td>
<td>34.00</td>
</tr>
<tr>
<td>4. Sheathing, Wood Fiber</td>
<td>0.03</td>
<td>0.500</td>
<td>20.00</td>
</tr>
<tr>
<td>5. Wood Fiber Board</td>
<td>0.03</td>
<td>0.500</td>
<td>26.00</td>
</tr>
<tr>
<td>6. Wood Fiber, hardboard type</td>
<td>0.12</td>
<td>0.500</td>
<td>65.00</td>
</tr>
<tr>
<td><strong>II Finish Flooring Materials</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Cork tile - ( \frac{3}{8} )&quot;</td>
<td>0.03</td>
<td>0.485</td>
<td>15.60</td>
</tr>
<tr>
<td>2. Terrazzo - 1&quot;</td>
<td>1.04</td>
<td>0.250</td>
<td>150.00</td>
</tr>
<tr>
<td><strong>III Insulating Materials</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>A. Blanket &amp; Batt</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Cotton Fiber</td>
<td>0.02</td>
<td>0.362</td>
<td>0.8-2.0</td>
</tr>
<tr>
<td>2. Mineral wool, fibrous form processed from rock, slag, or glass</td>
<td>0.03</td>
<td>0.30</td>
<td>0.5</td>
</tr>
<tr>
<td></td>
<td>0.02</td>
<td>0.30</td>
<td>1.5-4.0</td>
</tr>
<tr>
<td>3. Wood Fiber</td>
<td>0.02</td>
<td>0.30</td>
<td>3.2-3.6</td>
</tr>
<tr>
<td></td>
<td><strong>CON</strong> (Btu/hr·ft·°F)</td>
<td><strong>CP</strong> (Btu/lb·°F)</td>
<td><strong>ROW</strong> (lb/ft³)</td>
</tr>
<tr>
<td>----------------</td>
<td>------------------------</td>
<td>--------------------</td>
<td>-----------------</td>
</tr>
<tr>
<td><strong>B. Board &amp; Slabs</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Cellular Glass</td>
<td>0.03</td>
<td>0.185</td>
<td>9</td>
</tr>
<tr>
<td>2. Corkboard</td>
<td>0.02</td>
<td>0.485</td>
<td>6.5-8.0</td>
</tr>
<tr>
<td>3. Glass Fiber</td>
<td>0.02</td>
<td>0.185</td>
<td>4.9</td>
</tr>
<tr>
<td>4. Expanded rubber (rigid)</td>
<td>0.02</td>
<td>0.339</td>
<td>4.5</td>
</tr>
<tr>
<td>5. Expanded polyurethane (thickness 1 in. and greater)</td>
<td>0.02</td>
<td>0.20-0.25</td>
<td>1.5-2.5</td>
</tr>
<tr>
<td>6. Expanded polystyrene extruded</td>
<td>0.02</td>
<td>0.30-0.35</td>
<td>1.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td><strong>C. Loose Fill</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Mineral wool (glass, slag or rock)</td>
<td>0.03</td>
<td>0.30</td>
<td>2.0-5.0</td>
</tr>
<tr>
<td>2. Perlite (expanded)</td>
<td>0.03</td>
<td>0.378</td>
<td>5.0-8.0</td>
</tr>
<tr>
<td>3. Sawdust or shavings</td>
<td>0.04</td>
<td>0.30</td>
<td>0.8-15</td>
</tr>
<tr>
<td>4. Silica Aerogel</td>
<td>0.01</td>
<td>0.205</td>
<td>7.6</td>
</tr>
<tr>
<td>5. Vermiculite (expanded)</td>
<td>0.04</td>
<td>0.30</td>
<td>7.0-8.2</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>6. Wood Fiber, redwood, hemlock, or fir</td>
<td>0.02</td>
<td>0.30</td>
<td>2.0-3.5</td>
</tr>
<tr>
<td><strong>IV Masonry Materials</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Cement Mortar</td>
<td>0.42</td>
<td>0.271</td>
<td>116.0</td>
</tr>
<tr>
<td>2. Gypsum-fiber concrete</td>
<td>0.01</td>
<td>0.25</td>
<td>51.0</td>
</tr>
</tbody>
</table>

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### 3. Lightweight aggregates
including: expanded shale, clay, or slate; expanded slags; cinders; pumice; perlite; vermiculite; also cellular concretes

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Expanded Shale</td>
<td>0.43</td>
<td>0.20-0.25</td>
<td>120</td>
</tr>
<tr>
<td>Clay</td>
<td>0.30</td>
<td>0.20-0.25</td>
<td>100</td>
</tr>
<tr>
<td>Slate</td>
<td>0.21</td>
<td>0.20-0.25</td>
<td>80</td>
</tr>
<tr>
<td>Expanded Slags</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Cinders</td>
<td>0.14</td>
<td>0.20-0.25</td>
<td>60</td>
</tr>
<tr>
<td>Pumice</td>
<td>0.10</td>
<td>0.20-0.25</td>
<td>40</td>
</tr>
<tr>
<td>Perlite</td>
<td>0.08</td>
<td>0.20-0.25</td>
<td>30</td>
</tr>
<tr>
<td>Vermiculite</td>
<td>0.06</td>
<td>0.20-0.25</td>
<td>20</td>
</tr>
<tr>
<td>Cellular Concretes</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### 4. Stucco

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.42</td>
<td>0.20-0.25</td>
<td>116</td>
</tr>
</tbody>
</table>

### V Masonry Units

1. Brick, common

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.42</td>
<td>0.20</td>
<td>120</td>
</tr>
</tbody>
</table>

2. Brick, face

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.75</td>
<td>0.20</td>
<td>130</td>
</tr>
</tbody>
</table>

3. Clay tile, hollow

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1 cell deep</td>
<td>0.31</td>
<td>0.15</td>
<td>30</td>
</tr>
<tr>
<td>2 cells deep</td>
<td>0.33</td>
<td>0.15</td>
<td>30</td>
</tr>
<tr>
<td>2 cells deep</td>
<td>0.36</td>
<td>0.15</td>
<td>30</td>
</tr>
<tr>
<td>2 cells deep</td>
<td>0.38</td>
<td>0.15</td>
<td>30</td>
</tr>
<tr>
<td>3 cells deep</td>
<td>0.40</td>
<td>0.15</td>
<td>30</td>
</tr>
</tbody>
</table>

4. Concrete blocks, rectangular core

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sand and gravel aggregate</td>
<td>0.15</td>
<td>0.25</td>
<td>30</td>
</tr>
</tbody>
</table>

5. Stone, lime or sand

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>1.04</td>
<td>0.22</td>
<td>150</td>
</tr>
</tbody>
</table>

### VI Plastering Materials

1. Cement Plaster, sand aggregate

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.42</td>
<td>0.20</td>
<td>116</td>
</tr>
</tbody>
</table>

2. Gypsum Plaster

<table>
<thead>
<tr>
<th></th>
<th>CON (Btu/hr-ft-°F)</th>
<th>CP (Btu/lb-°F)</th>
<th>ROW (lb/ft³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Perlite aggregate</td>
<td>0.12</td>
<td>0.20</td>
<td>45</td>
</tr>
<tr>
<td>Sand aggregate</td>
<td>0.47</td>
<td>0.20</td>
<td>105</td>
</tr>
<tr>
<td>Vermiculite aggregate</td>
<td>0.01</td>
<td>0.20</td>
<td>45</td>
</tr>
</tbody>
</table>

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G-3
VII Roofing

1. Asbestos-cement shingles 0.40 0.20 120
2. Asphalt roll roofing 0.54 0.20 70
3. Asphalt shingles 0.19 0.20 70

VIII Siding Materials (on flat surfaces)

1. Shingles - asbestos-cement 0.40 0.20 120
2. Siding
   asbestos-cement - \( \frac{1}{4} \) 0.10 0.20 120
   asphalt roll siding 0.54 0.20 120
3. Architectural glass 0.83 0.15-0.20 150-175

IX Woods

1. Maple, oak, and similar hardwoods 0.09 0.50 45
2. Fir, pine and similar softwoods 0.07 0.50 32

CONFIGURATION

<table>
<thead>
<tr>
<th>Thermal Conductivity Unit Distance</th>
<th>Specific Heat</th>
<th>Density</th>
</tr>
</thead>
<tbody>
<tr>
<td>CON/DX (Btu/hr-ft-°F)</td>
<td>CP (Btu/lb-°F)</td>
<td>ROW (lb/ft³)</td>
</tr>
<tr>
<td>I Vertical Space</td>
<td>1.03</td>
<td>0.24</td>
</tr>
<tr>
<td>II Horizontal Space</td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Heat flow up</td>
<td>1.18</td>
<td>0.24</td>
</tr>
<tr>
<td>2. Heat flow down</td>
<td>1.01</td>
<td>0.24</td>
</tr>
<tr>
<td>III 45° Inclined Space</td>
<td></td>
<td></td>
</tr>
<tr>
<td>1. Heat flow up</td>
<td>1.11</td>
<td>0.24</td>
</tr>
<tr>
<td>2. Heat flow down</td>
<td>1.13</td>
<td>0.24</td>
</tr>
</tbody>
</table>

GENERAL AMERICAN RESEARCH DIVISION
### SOIL

<table>
<thead>
<tr>
<th></th>
<th>Thermal Conductivity (Btu/hr-ft(^{\circ})F)</th>
<th>Specific Heat CP (Btu/lb(^{\circ})F)</th>
<th>Density ROW (lb/ft(^3))</th>
</tr>
</thead>
<tbody>
<tr>
<td>I</td>
<td>0.96</td>
<td>0.188</td>
<td>100.00</td>
</tr>
<tr>
<td>II</td>
<td>0.83</td>
<td>0.210</td>
<td>100.00</td>
</tr>
<tr>
<td>III</td>
<td>0.75</td>
<td>0.200</td>
<td>110.00</td>
</tr>
<tr>
<td>IV</td>
<td>0.50</td>
<td>0.190</td>
<td>100.00</td>
</tr>
<tr>
<td>V</td>
<td>0.46</td>
<td>0.230</td>
<td>100.00</td>
</tr>
<tr>
<td>VI</td>
<td>0.54</td>
<td>0.210</td>
<td>110.00</td>
</tr>
<tr>
<td>VII</td>
<td>0.42</td>
<td>0.195</td>
<td>100.00</td>
</tr>
<tr>
<td>VIII</td>
<td>0.37</td>
<td>0.210</td>
<td>100.00</td>
</tr>
<tr>
<td>IX</td>
<td>0.33</td>
<td>0.220</td>
<td>100.00</td>
</tr>
<tr>
<td>X</td>
<td>0.42</td>
<td>0.220</td>
<td>90.00</td>
</tr>
<tr>
<td>XI</td>
<td>0.42</td>
<td>0.200</td>
<td>90.00</td>
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</table>

### BOUNDARY ORIENTATION

<table>
<thead>
<tr>
<th></th>
<th>Direction of Heat Flow</th>
<th>Film Heat-Transfer Coefficient</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Into or out of shelter</td>
<td>HI, HQ (Btu/hr-ft(^{\circ})F)</td>
</tr>
<tr>
<td>I</td>
<td>Vertical</td>
<td>1.46</td>
</tr>
<tr>
<td>II</td>
<td>Horizontal (ceiling)</td>
<td>1.08</td>
</tr>
<tr>
<td></td>
<td>Into shelter</td>
<td>1.63</td>
</tr>
<tr>
<td>III</td>
<td>Horizontal (floor)</td>
<td>1.63</td>
</tr>
<tr>
<td></td>
<td>Into shelter</td>
<td>1.08</td>
</tr>
<tr>
<td></td>
<td>Out of shelter</td>
<td></td>
</tr>
</tbody>
</table>

GENERAL AMERICAN RESEARCH DIVISION

G-5
APPENDIX H

SHEP CODE, MODIFICATION 3

FLOW CHART AND LISTING
START

READ INPUT DATA (SECTION 3)

CALCULATE INTENSITY OF SOLAR RADIATION (SECTION 2.2, APPENDIX B)

IS SHELTER AIR-CONDITIONED?

HAS OCCUPANCY TERMINATED?

CALCULATE ENERGY TRANSFER DUE TO AIR-CONDITIONING (SECTION 2.3, APPENDIX F)

ARE BOUNDARIES ADIABATIC?

CALCULATE ENERGY TRANSFER THROUGH BOUNDARIES (SECTIONS 2.1, 2.4, APPENDICES C, D, E)

CALCULATE METABOLIC ENERGIES (SECTION 2.5)

CALCULATE SHELTER ENVIRONMENTAL CONDITIONS (SECTIONS 9, 10, APPENDIX A)

PRINT RESULTS
PROGRAM SHEP

SHELTER ENVIRONMENTAL PREDICTION CODE (SHEP-MOD. 3)

GENERAL AMERICAN RESEARCH DIVISION

GENERAL AMERICAN TRANSPORTATION CORPORATION


COMMON/MATRIX/AINV(40,40,20)

DIMENSION TWALL(40,20,40,40),INDEX(40,1,40),T(40)

DIMENSION EQTIM(365),TD2P(336),TWB(336),TEFF(336)

DIMENSION PSAT(120),IN(5,20),DP(5,20),DX(5,20),ALPHA(5,20),CON(5,20)

DIMENSION ROW(5,20),CP(5,20),CW(20)

DIMENSION INT(60),QS(2,20),BB(40),BMUL(40,20),TDI(30),TWI(30),TEI(30),TDIAV(30),TWIAV(30),TEIAV(30),TSOIL(20)

DIMENSION XI(20),AZ(20),LAYMAX(20),QLATC(20),HI(20),HO(20),NMAX(20)

DIMENSION ITWALL(20),QSW(20),QG(20),AREA(20),TDD(14),TWD(14),TED(14),TDAVG(14)

DIMENSION ITWAVG(14),TEAVG(14),IDATA(13),LST(2),TRANS(20),ASOIL(20)

3AJIT(20)

JJJJ=1

INITIALIZE ALL MATRIX ELEMENTS TO ZERO.

1311 DO 1 I=1,40

DO 1 J=1,40

DO 1 K=1,20

1 AINV(I,J,K)=0.0

DO 2 I=1,40

T(I)=0.0

DO 2 J=1,2

INDEX(I,J)=0

DO 3 I=1,40

DO 3 J=1,20

BMUL(I,J)=0.0

3 TWALL(I,J)=0.0

DO 5 I=1,365

5 EQTIM(I)=0.0

DO 6 I=1,336

6 TD2P(I)=TWB(I)=TEFF(I)=0.0

DO 7 I=1,120

7 PSAT(I)=0.0

DO 8 I=1,5

DO 8 J=1,20

INT(I,J)=0

8 DP(I,J)=DX(I,J)=ALPHA(I,J)=CON(I,J)=ROW(I,J)=CP(I,J)=0.0

DO 9 I=1,60

9 INT(I,J)=0

DO 10 I=1,2

DO 10 J=1,20

10 QSW(I,J)=0.0

302 TD(I)=TW(I)=TEI(I)=TDIAV(I)=TWIAV(I)=TEIAV(I)=0.0

DO 303 I=1,20

CW(I)=0.0
LAYMAX(I)=NMAX(I)=ITWALL(I)=0
303 XI(I)=AZ(I)=GLATC(I)=HI(I)=HO(I)=QSW(I)=QW(I)=AREA(I)=TRANS(I)=ASO
1I(I)=TSOIL(I)=AJUT(I)=0=Q
DO 304 I=1,14
304 TDD(I)=TWD(I)=TED(I)=TDAVG(I)=TWAVG(I)=TEAVG(I)=0.0
DO 305 I=1,13
305 IDATA(I)=0
DO 306 I=1,2
306 LST(I)=0

C READ INPUT DATA AND SET CONSTANTS
C
307 DO 11 I=1,365
11 READ 1007*EQTIM(I)
DO 12 I=501,120
12 READ 1001*PSAT(I)
308 READ 1006*IDATA
READ 1003*ALT=ALAT=ALONG=NW+GG+HM+WP+F1+QLITE+LDSOIL,DO*HRS=LST(I)
1*NOINT
DO 16 J=1,NW
READ 1020*AREA(J)+LAYMAX(J)+NMAX(J)+HI(J)+HO(J)+ASOIL(J)
IF(MAX(D(I)=11312+15+15
1312 READ 1001*TRANS(J)+XI(J)
IF(XI(J)=10,014+15,999
14 READ 1003*AZ(J)
15 LEM=LAYMAX(J)
DO 16 K=1,LEM
16 READ 1009*DP(K,J)+DX(K,J)+CON(K,J)+ROW(K,J)+CP(K,J)
READ 1013*CFMIN+TCOI+L+VCOIL+BF+F2+TD2+R2+TWB(I)+TEFF(I)
DO 18 K=1,NW
IF(ASOIL(J)=18,18,1703
1703 READ 1008*TSOIL(J)
18 CONTINUE
IF(IDATA(I)=19,19,21
19 READ 1008*TO
DO 20 J=1,NW
NEM=NMAX(J)+1
DO 20 K=1,NEM
20 TWALL(K,J)=TO
GO TO 22
21 DO 22 J=1,NW
NEM=NMAX(J)+1
DO 22 K=1,NEM
22 TWALL(K,J)=TO
23 READ 1001*DT
IHS=HRS
NODAYS=IHRS/24
IF(NOINT(1)=1701+1701+1702
1702 NOD=2*NOINT
DO 17 I=1,NOD
17 READ 1006*INT(I)
1701 ID=D
LNM=25
1
KIND=0
GLH=0.0
ADT=0.0
IHRMG=1
NTAU=0
C
CALCULATE INTENSITY OF SOLAR RADIATION FOR EACH EXPOSED BOUNDARY
C
25 LST(2)=LST(1)+1
DO 53 I=1,2
LSTM=LST(I)
251 DO 53 J=1,NW
IF(ASOIL(J))252,53,53
252 IF(IDATA(10))26,26,27
26 C2=294.
C3=3.183
GO TO 28
27 C2=200.
C3=2.228
28 IF(X1(J))90.,29,29,999
29 ETAR=0.410152*SINF(ID-80)*PI/182.5
S1=TANF(ETAR)
S2=SINF(ETAR)
S3=COSF(ETAR)
PHIR=ALAT/ON
S4=TANF(PHIR)
S5=SINF(PHIR)
S6=COSF(PHIR)
AZR=AZ(J)/ON
XIR=X1(J)/ON
S7=COSF(XIR)
S8=SINF(XIR)
IF(PHIR=(PI*0.5))30,998,998
30 IF(ETARGPHIR=(PI*0.5))31,998,998
31 IF(ETAR)34,34,32
32 IF(PHIR=(PI*0.5-ETAR))34,33,33
33 THETAR=0.0
GO TO 35
34 THETAR=ACOSF(S4*S1)
35 THETAS=2.*PI-THETAR
IN=ALONG/15
TI=LSTM6EQTIM(ID)-ALONG/15*06IN
THETA=OM+TI
S9=COSF(THETA)
IF(THETA-THETAR)36,37,37
36 DIR=0.0
DIF=0.0
GO TO 52
37 IF(THETA-THETAS)38,38,36
38 BETAR=ASINF(S5*S2-S6*S9*S3)
S10=COSF(BETAR)
S11=SINF(BETAR)
IF(BETAR)39,39,39
39 IF(BETAR=(PI*0.5))392,391,392
391 GAMMAR=AAR
GO TO 393
GAMMAR*ACOSF((1-IS10*(S6*S26*S5*S9*S3))
IF(GAMMAR) 40,40,41
GAMMAR=GAMMAR+PI
DIRNORM=C2*(1-EXP(-C3*BETAR))
S13=S10*COSF(GAMMAR-AZR)
ALPHAR=ACOSF(S13*S76811*S8)
S12=COSF(ALPHAR)
IF(ALPHAR=(PI*0.5)) 43,43,42
DIR=0.0
GO TO 49
IF(S13) 45,44,44
FALPHA=0.35*S13**2+0.60*45*S130.55
GO TO 48
IF(S130.04) 47,47,46
FALPHA=0.625*S13**2+0.525*S130.5
GO TO 48
FALPHA=0.44
DIR=DIRNORM*S12
DIFF=S11*FALPHA+1.11.*S81*S81
DIF2=0.677E-06*DIRNORM**2-1.5E-04*DIRNORM+0.0183
DIF=DIF1/DIF2
T0=DIR&DIFF
QSI+J)=TOT
CONTINUE
QST=0.0
QSO=0.0
DO 54 J=1*NW
QSW(J)=QSI+2+J)
QSW=TRANS(J)*QSW(J)*AREA(J)*QSO
QST=QST+QSW(J)*AREA(J)
C FOR EACH HOUR OF OCCUPANCY AFTER THE FIRST, RESET HOUR NUMBER AND SET
C CONDITIONS AT THE END OF THE PRECEDING HOUR TO THOSE AT THE BEGINNING
C OF THE SUCCEEDING HOUR. READ THE INLET CONDITIONS FOR THE SUCCEEDING HOUR.
C
IF(IHRNO=157,24,57
DO 56 J=1*NW
QSI=QSI+J)
IHRNO=IHRNO1
LSTM=LSTM1
IF(24=LSTM)5612+5612+251
5612 LSTM=0
ID=1D1
IF(365-ID)5612+251+251
5611 ID=1
GO TO 251
57 TD11=TD12
R11=R12
TA1=TA2
ADT=DT
IF(I(DATA(12))181,181,182
181 READ 1018+PP1*CFIN+QGLES+QEQIHP
182 IF(I(DATA(13))183,183,60
183 READ 1019+TD12+TA2+R12
GO TO 60
58 QST=0.0
QSO=0.0
DO 59 J=1*NW
QSO=QSO+J)6ADT*(QSI+J)-QSI+J))
QSW(J)=QSO
592657**.c
QSOLAR = TRANS(J) * QSW(J) * AREA(J) * GSOLAR
59 QST = QST + QSO

C FOR TIME INCREMENTS DURING THE HOUR, DETERMINE INLET CONDITIONS AS A LINEAR INTERPOLATION BETWEEN HOURLY VALUES.

C
60 TD1 = TD11 + ADT * (TD11 - TD12)
    R1 = R11 + ADT * (R11 - R12)
    PG = 5.132 * EXP (0.329 * TD1)
    PGPP = R1 * PG
    BP = 0.986 * 0.0759 * ALT * 2
    W1 = (0.062 * PGPP) / (BP - PGPP)
    TA = TA1 + ADT * (TA1 - TA2)
    LL = 1

C CALCULATE NEW INLET CONDITIONS WITH AIR-CONDITIONING. DETERMINE PROPERTIES OF THE INLET AIR FOR THE BEGINNING OF THE TIME INCREMENT.

C
IF (DATA(7)) 403 * 403 * 402
402 TD1 = TD26 * (F2 / F1) * (TD1 - TD2)
    PGPP = 5.132 * R2 * EXP (0.329 * TD2)
    W2 = (0.062 * PGPP) / (BP - PGPP)
    W1 = W2 (F2 / F1) * (W1 = W2)
    ADMIX = (1 - CFMIN) / (W1 = WCOIL)
    TDA = TCOIL * ADMIX * (TD1 - TCOIL)
    WA = WCOIL * ADMIX * (W1 = WCOIL)
    E1 = EX (0.0329 * TDA)
    PGPP = WA / BP / (W60 * 622)
    PG = 5.132 * E1
    R1 = PGPP / PG
    WAC = 60.0 * CFMIN * DT * (0.02874 * BP - 0.0962 * R1 * E1) / (TD649 * 69)
    HF = 1093.9 * 0.567 * TCOIL
    PAIRCOND = 0.24 * WAC * (TD1 - TDA) / DT6WAC * (W1 - WA) * HF / DT
    TD1 = TDA
    W1 = WA
    GO TO 61

403 PAIRCOND = 0 * 0
61 E1 = EX (0.0329 * TD1)
    E2 = EX (0.0329 * TD2)
    HAS1 = 0.24 * TD2
    HVSI1 = 1061.0 * 60.0 * 444 * TD2
    HAI1 = 0.24 * TD1
    HV1 = 1061.0 * 60.0 * 444 * TD1
    HFG = 1093.9 * 0.567 * TD2
    WAS1 = V5 * (0.01874 * BP - 0.0962 * R2 * E2) / (TD26459 * 69)
    WVS1 = V5 * (0.05987 * R2 * E2) / (TD26459 * 69)
    WA1 = 60.0 * FI1 * DT * (0.01874 * BP - 0.0962 * R1 * E1) / (TD16499 * 69)
    WV1 = 60.0 * FI1 * DT * (0.05987 * R1 * E1) / (TD16499 * 69)
    HAS1 = HAS1 + WVS1 * HVSI1
    H1 = WA1 * HAI1 + WV1 * HV1
    WAO = WA1 + WAS1

C CALCULATE THE HEAT TRANSFER THROUGH THE BOUNDARIES DUE TO TEMPERATURE DIFFERENCES AND DUE TO MOISTURE CONDENSATION.

C
IF (DATA(6)) 69 * 69 * 70
69 QWC = 0.0
QLH = 0.0
NTAU = NTAU + 1
IHRN = IHRNO - 1
GO TO 146
70  DO 71  J=1, NW
     I LL=0
     LEM=LAYMAX(J)
     DO 71  K=1,LEM
     IN(K, J)=DP(K, J)/DX(K, J)+16*ILL
71  I LL=IN(K, J)
     J WALL=1
     LAY=1
     I =1
72  NEM=NMAX(JWALL+1)
     DO 4  INA=1, NEM
     DO 4  JNA=1, NEM
     A(INA, JNA)=0.0
     B(INA, JNA)=0.0
80
71  ALPHA(LAY*JWALL) = CO N (LAY*JWALL)/(ROW(LAY*JWALL)*CP(LAY*JWALL))
     BAS1=1.0*CON(LAY+1*JWALL)*D X(LAY*JWALL)/(DX(LAY+1*JWALL)*CO N(LAY+1*JWALL))
     GROW(LAY*JWALL)*CP(LAY*JWALL)*DX(LAY*JWALL)++2/(2.0*CON(LAY+1*JWALL))
     ROW(LAY*JWALL)*DT
     J WALL=1
     I T D2=TD2
     PS=PSAT(ID T D2),ID T D2=IT D2) = (PSAT(ID T D2)+PSAT(ID T D2))
     PO=PS*R2
     I TWALL(JWALL)=TWALL(1, JWALL)
     I ELF1=I TWALL(JWALL)
     I ELF2=TWALL(1, JWALL)
     PSW=PSAT(I ELF1) & I ELF2=I ELF1) *(PSAT(I ELF161) - PSAT(I ELF1))
     TENV=T D2&T W A L L (1, JWALL))/2.0
     ROAIR=3.25E-07* TENV**2.0-1.86E-04* TENV**0.063
     C=2.0*28292H*H(I JW ALL )*PO/(BP*PO)=PSW/(BP*PSW)/ROAIR
     CM(JWALL)=C*A REA (JWALL)*DT/HFG
     IF(CM(JWALL))=772, 79, 771
771  AJIT(JWALL)=AJIT(JWALL)+C*CM(JWALL)
     GO TO 79
772  IF(A BSF(CM(JWALL)))=AJIT(JWALL)=771, 771, 774
774  CM(JWALL)=AJIT(JWALL)
     C=CM(JWALL)+HFG/(AREA(JWALL)*DT)
     GO TO 771
79  QL AT C(JWALL)=C
     IF(NTAU)=90*80+81
80  AI (I)=1.0*CON(LAY*JWALL)/(H I(JWALL)*DX(LAY*JWALL)) & G R O W (L AY*JWALL)
     I =CO N(LAY+1*JWALL)*D X(LAY*JWALL)/(2.0*HI(I JW ALL )*D T)
     AI (I)=CON(LAY*JWALL)/(H I(JWALL)*D X(LAY*JWALL))
81  BB(I)=ROW(LAY*JWALL)*CP(LAY*JWALL)*DX(LAY*JWALL)/(2.0*HI(I JW ALL )*D T)
     1*TW ALL(1, JWALL)*IT D 26C/H I(JW ALL)
     I =16
82  IF(I=IN(LAY*JWALL)) = 83, 83, 86
83  IF(NTAU)=84*84+85
84  AI (I)=1.0
     AI (I)=DX(LAY*JWALL)**2/(ALPHA(LAY*JWALL)*DT) & 62
     AI (I)=1.0
85  BB(I)=DX(LAY*JWALL)**2*T W A L L (1, JWALL)/(ALPHA(LAY*JWALL)*D T)
     I =16
     GO TO 82
86  IF(LAY=LAYMAX(JWALL)) = 87, 90*996
87  IF(NTAU)=88*88+89
88  AI (I)=1.0
     AI (I)=BAS1
     AI (I)=CON(LAY*JWALL)*DX(LAY*JWALL)/(DX(LAY+1*JWALL)*CON(LAY+1*JWALL))
89  BB(I)=ROW(LAY*JWALL)*CP(LAY*JWALL)*DX(LAY*JWALL)**2*ROW(LAY+1*JWALL)

1AIL1*CP(LAY61*JWALL)*DX(LAY*JWALL)*DX(LAY61*JWALL))*TWALL(I,JWALL)
2*(2.0*CON(LAY*JWALL)*DT)
I=61
LAY=LAY61
IF(LAY-LAYMAX(JWALL)=721,721.0)
90 IF(A(SOIL(JWALL))91,92,96
91 TAJ=TA
GO TO 93
92 TAJ=0.5*(TD26*TA)
93 IF(NTAU)94,94,95
94 A(I+I-1)=CON(LAY,JWALL)*(HO(JWALL)*DX(LAY,JWALL))
A(I+I)=A(I+I-1)*61*6GROW(LAY,JWALL)*DX(LAY,JWALL)*CP(LAY,JWALL)/(2
1.0*HO(JWALL)*DT)
95 IF(A(SOIL(JWALL))951,952,96
951 BB(I)=(1.0-TRANS(JWALL))*(OSW(JWALL)/HO(JWALL))*TAJ&ROW(LAY,JWALL)*C
1P(LAY,JWALL)*DX(LAY,JWALL)/(2.0*DT*HO(JWALL))*TWALL(I,JWALL)
GO TO 103
952 BB(I)=TAJ&ROW(LAY,JWALL)*CP(LAY,JWALL)*DX(LAY,JWALL)/(2.0*DT*HO(JW
ALL))TWALL(I,JWALL)
GO TO 103
96 IF(I-NMAX(JWALL)-1)100,100,996
100 TWALL(I,JWALL)*TSOIL(JWALL)
HARRY=ROW(LAY,JWALL)*CP(LAY,JWALL)*DX(LAY,JWALL)**2/(CON(LAY,JWALL)
I)*DT)
IF(NTAU)101,101,102
101 A(I+I-1)=1.0
A(I+I)=2.0*G&HARRY
102 BB(I)=HARRY*TWALL(I,JWALL)*TSOIL(JWALL)
103 IF(NTAU)104,104,1351
104 NEM=NMAX(JWALL)61
DO 108 I=1,NEM
108 INDEX(I+1)=0
II=0
109 AMAX=-1
DO 110 I=1,NEM
IF(INDEX(I+1))110,111,110
111 DO 112 J=1,NEM
IF(INDEX(J+1))112,113,112
113 TEMP=ABS(A(I+J))
IF(TEMP-AMAX)112,112,114
114 IROW=I
ICOL=J
AMAX=TEMP
112 CONTINUE
110 CONTINUE
IF(AMAX)225,115,116
115 PRINT 133
133 FORMAT(11H ZERO PIVOT)
GO TO 69
116 INDEX(ICOL+1)=IROW
IF(IROW-ICOL)119,118,119
119 DO 120 J=1,NEM
TEMP=A(IROW+J)
A(IROW+J)=A(ICOL+J)
120 A(ICOL+J)=TEMP
II=II+1
INDEX(I+2)=ICOL
118 PIVOT=A(ICOL+ICOL)
A(ICOL+ICOL)=1.0
PIVOT=1.0/PIVOT
DO 121 J=1,NEM
121 A(I*COL+J)=A(I*COL+J)+P*O
DO 122 I=1,NEM
122 IF(I*COL+123)=122+123
123 TEMP=A(I*COL+1)
A(I*COL+1)=0.0
DO 124 J=1,NEM
124 A(I*J)=A(I*J)+A(I*COL+J)*TEMP
DO 125 I=1,NEM
126 A(I*COL)=TEMP
II=II+1
127 IF(II)=125,127,125
DO 126 I=1,NEM
127 BMU(I+JWALL)=BB(I)
DO 128 J=1,NEM
128 AINV(I+JWALL)=A(I+J)
129 IF(JWALL)=NW,143+142+995
130 JWALL=JWALL+1
131 I=1
132 LAY=1
GO TO 72
133 DO 134 K=1,NW
134 QW(K)=HI(K)*AREA(K)*(TD2-TWALL(K))
QWC=0.0
QLH=0.0
DO 135 J=1,NW
135 QW=QWC+QW(J)
136 QH=QLH*QLAT(J)*AREA(J)
137 C C CALCULATE METABOLIC HEAT ENERGIES
138 C
139 NTAU=NTAU+1
140 IHRN=IHRNO-1
141 IF(TEFF(IHRNO)-87.0)=149+149+147
142 IF(TEFF(IHRNO)-102.0)=148+148+994
143 QRT=1.508*TEFF(IHRNO)**2.259+7.259*TEFF(IHRNO)-10.795+2
GO TO 151
144 IF(TEFF(IHRNO)-50.0)=193+150+150
145 QT=1.482*TEFF(IHRNO)+6514+0
146 IF(TD2-50.0)=192+152+152
147 QSENS=-0.06875*TD2**2+625.625*TD2+523.0
148 QSEN=QSENS+P
149 QL=QL*P
150 C C CALCULATE THE SHELTER DRY-BULB TEMPERATURE AND RELATIVE HUMIDITY AT THE END OF THE TIME INCREMENT
151 IF(R-1.0)=154+155+155
152 QL=QL*R
153 PRINT 2001,IHRN,R
154 DO=HS16H*QSENSQL*(HVS1/HFG)=QW*QL+QEQ=EQUIP+PAIRQND+GSOER+QLM
155 WVL=QW/DT/HFG
WVCOND=QLH*DT/HFG
WVO=WV16WVL&WVS1-WVCOND
IF (WVCOND) 1554, 1554, 1556
1556 IF (WVO) 1553, 1554, 1554
1553 WVO=0.0
1554 TD2P(IHRNOI)=(DO-1061.0*WVO)/(0.444*WVO60+24*WAO)
1552 IF (ABSFGIL=TD2P(IHRNOI)-1.00) 1552, 1551, 1551
1551 IF (TD2P(IHRNOI)-50.0) 156, 156, 156
1556 IF (WVO) 1561, 1561, 1563
1561 PV2=0.0
1562 R2P=0.0
GO TO 1562
1563 PV2*BP/(0.622*WAO/WVO61+0)
EPS*EXPF(0.0329*TD2P(IHRNOI))
1561 PV2=0.0
1562 R2P=0.0
GO TO 1562
1563 PV2*BP/(0.622*WAO/WVO61+0)
EPS*EXPF(0.0329*TD2P(IHRNOI))
R2P=PV2/(5.132*EPS)
1562 IF (R=0.0) 157, 157, 158
157 R2P=1.0
GO TO 157
158 IF (MOND=2) 159, 160, 160
159 MOND=2
160 IF (R2P=1.0) 162, 162, 161
161 R=R+DR
GO TO 153
162 R=R+DR
DR=0.1*DR
MOND=MOND+1
163 IF (LL=IDATA(3)) 1555, 1555, 991
164 TD2=0.5*(TD2&TD2P(IHRNOI))
GIL=TD2
1555 TWALL(I)=TC(I)
1555 IF (R2P=1.0) 167, 167, 990
166 TWB(IHRNO)=TD2P(IHRNO)
TEFF(IHRNO)=TD2P(IHRNO)
GO TO 168
167 TWO=TD2P(IHRNO)
DWO=10.0
MM=0
168 PSS=5.132*EXPF(0.0329*TWO)
TWB(IHRNO)=((BP-PSS)*TD2P(IHRNO)-2800.0*(PSS-PV2))/(BP-61.3*P
1V2-2.3*PSS)
169 IF(TWB(IHRNO)-TWO) 170, 171
170 TWO=TWO-DWO
GO TO 168
171 TWO=TWO&DWO
DWO=0.1&DWO
MM=MM61
172 TEF1=107.5*(TD2P(IHRNO)-TWB(IHRNO))+62.3*TWB(IHRNO)
TEFF(IHRNO)=TEF1/(62.3*TD2P(IHRNO)+TWB(IHRNO))
C PRINT RESULTS FOR THE HOUR.
C IF(KIND=IDATA(5)) 173, 174, 989
173 KIND=KIND61
GO TO 180
174 IF(IDATA(11)) 177, 178, 175
175 IF(IHRNO-1) 179, 187, 987
176 PRINT 2002
PRINT 2037
PRINT 2003
PRINT 2004
PRINT 2005
PRINT 2006
PRINT 2030
PRINT 2031
177 IF(IHRNO=LMN) 1772, 1771, 1772
1771 LMN=LMN624
PRINT 2038
1772 F3=F1/P
PRINT 2006*IHRNO*F3+TD2P(IHRNO)+TWB(IHRNO)+TEFF(IHRNO)*PAIRCOND*QW
1C+QLH+QSLAR+QSen+QL+QITE+QEQUIP
178 IF(IHRNO-IHRS) 179, 187, 987
179 KIND=1
180 TD2=TD2P(IHRNO)
R2=R2P
ADT=ADT6DT
TEFF(IHRNO61)=TEFF(IHRNO)
24 IF(ADT=1.00001) 58, 59, 55
C ERROR MESSAGES
C 999 PRINT 2007+JX(1)
GO TO 5000
998 PRINT 2008
GO TO 5000
997 PRINT 2009
GO TO 5000
996 PRINT 2010
GO TO 5000
995 PRINT 2011
GO TO 5000
994 PRINT 2012*IHRN*TEFF(IHRNO)
GO TO 148
993 PRINT 2012*IHRN*TEFF(IHRNO)
GO TO 150
992 PRINT 2014*IHRN*TD2P(IHRNO)
GO TO 152
991 PRINT 2015
GO TO 165
990 PRINT 2016
GO TO 166
989 PRINT 2017
   GO TO 174
988 PRINT 2018
   GO TO 176
987 PRINT 2019
   GO TO 187
986 PRINT 2036*TD2P(1),IHRN
   GO TO 156

C CALCULATE AND PRINT TIME-AVERAGE SHELTER TEMPERATURES.

187 TDMAX=TD2P(1)
   LM=1
188 DO 190 L1=1,IHM
   IF(TDMAX-TD2P(L1))>109,190
189 TDMAX=TD2P(L1)
   LM=L1
190 CONTINUE
   PRINT 2020*TDMAX,LM
   TDMIN=TD2P(1)
   LM=1
191 DO 193 L1=1,IHM
   IF(TDMIN-TD2P(L1))>193,192
192 TDMIN=TD2P(L1)
   LM=L1
193 CONTINUE
   PRINT 2032*TDMIN,LM
   TWMAX=TWB(1)
   LM=1
194 DO 196 L1=1,IHM
   IF(TWMAX-TWB(L1))>195,196
195 TWMAX=TWB(L1)
   LM=L1
196 CONTINUE
   PRINT 2021*TWMAX,LM
   TWMIN=TWB(1)
   LM=1
197 DO 199 L1=1,IHM
   IF(TWMIN-TWB(L1))>199,198
198 TWMIN=TWB(L1)
   LM=L1
199 CONTINUE
   PRINT 2033*TWMIN,LM
   ETMAX=TEFF(1)
   LM=1
200 DO 202 L1=1,IHM
   IF(ETMAX-TEFF(L1))>201,202
201 ETMAX=TEFF(L1)
   LM=L1
202 CONTINUE
   PRINT 2022*ETMAX,LM
   ETMIN=TEFF(1)
   LM=1
203 DO 205 L1=1,IHM
   IF(ETMIN-TEFF(L1))>205,204
204 ETMIN=TEFF(L1)
   LM=L1
205 CONTINUE
   PRINT 2034*ETMIN,LM
PRINT 2023
PRINT 2024
TDW=0.0
TWW=0.0
TEW=0.0
DO 213 J=1,1HRS
TDW=TDW+TD2P(J)
TWW=TWW+TWB(J)
213 TEW=TEW+TEFF(J)
TDS=TDW/HRS
TWS=TWW/HRS
TES=TEW/HRS
PRINT 2035+TDS+TWS+TES
IF(INODAYS)5000,209,206
206 LB=1
LE=24
DO 2071 IDAY=1,NODAYS
DO 207 J=LB,LE
TDD(IDAY)=TDD(IDAY)+TD2P(J)
TWD(IDAY)=TWD(IDAY)+TWB(J)
207 TED(IDAY)=TED(IDAY)+TEFF(J)
LB=LB+24
2071 LE=LE+24
PRINT 2025
TDAVG(IDAY)=TDAVG(IDAY)+TDD(IDAY)/24.0
TAVG(IDAY)=TAVG(IDAY)+TWD(IDAY)/24.0
TEAVG(IDAY)=TEAVG(IDAY)+TEDE(IDAY)/24.0
208 PRINT 2026+IDAY*TDAVG(IDAY)+TAVG(IDAY)+TEAVG(IDAY)
209 IF(NOINT)=5000,5000,210
210 PRINT 2027
ND=2*NOINT-1
DO 212 NI=1,ND+2
MM=(NI+1)/2
ILT=INT(NI)
ILL=INT(NI+1)
DO 211 MI=ILT+ILL
TDI(MM)=TDI(MM)+TD2P(MI)
TWI(MM)=TWI(MM)+TWB(MI)
211 TEI(MM)=TEI(MM)+TEFF(MI)
TDIAV(MM)=TDI(MM)/INT(NI+1)-INT(NI)+1
TWIAV(MM)=TWI(MM)/INT(NI+1)-INT(NI)+1
TEIAV(MM)=TEI(MM)/INT(NI+1)-INT(NI)+1
212 PRINT 2028+INT(NI+1)*INT(NI+1)+TDIAV(MM)+TWIAV(MM)+TEIAV(MM)
186 JJJ=JJJ+DATA(4)+186+5000+5000
GO TO 1311

C

1001 FORMAT(F7.3,F7.1)
1003 FORMAT(F7.1,F4.1*F5.1+F5.1*123*F7.1*F5.0*F9.2*2*F8.1*2*F3.0+12)
1006 FORMAT(1313)
1007 FORMAT(F5.2)
1008 FORMAT(F4.1)
1009 FORMAT(2F6.3*2F6.2*F6.3)
1013 FORMAT(F9.2*F4.1+F8.5*F4.2+2*F9.2+2*F4.1*2*F4.1)
1018 FORMAT(F5.0*2*F9.2*2*F8.1)
1019 FORMAT(2F4.1*F5.2)
1020 FORMAT(F7.1+2*F5.2*F3.0)
1021 FORMAT(4F4.1*2*F5.2)
DURING HOURS IS \( \approx 1.3 \times 10^7 \) WHICH IS LESS THAN 1.0

THEREFORE, THE LATENT ENERGY INTRODUCED BY THE OCCUPANTS HAS BEEN REDUCED.

THEATENT ENERGY INTRODUCED BY THE OCCUPANTS HAS BEEN REDUCED TO THE NOMINAL OCCUPANT ACTIVITY LEVEL \( 1.0 \times 400 \) BTU/HR.

LOADS \( C_B T U/HR \) * VENT \( C_B T U/HR \) *

METABOLIC ENERGY \( \eta \)

TIME RATE DBT WBT ET

BOUNDARY EQUIPMENT

TIME- AVERAGE TEMPERATURE VALUES

FOR ENTIRE DURATION OF OCCUPANCY \( 16X \times DBT \times 7X \times WB1 \times 6X \times ET \)

FOR EACH DAY OF OCCUPANCY \( 15X \times MAX \) DRY-BULB TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

WET-BULB TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

EFFECTIVE TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

TIME-AVERAGE TEMPERATURE VALUES

MIN. DRY-BULB TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

MIN. WET-BULB TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

MIN EFFECTIVE TEMP. DURING OCCUPANCY \( 14X \times 6X \times F4 \times 1 \) AT 1H \( 14 \) HOURS AFTER BEGINNING OF OCCUPANCY*

TD2Pa \( \approx 1.1 \times 10^8 \) AT 1H

VALUES ARE FOR LAST TIME INCREMENT OF EACH HOUR

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**Title:** SHELTER ENVIRONMENTAL PREDICTION (SHEP) COMPUTER CODE, MODIFICATION 3

**Abstract:**

The Shelter Environmental Prediction (SHEP) Computer Code, Mod. 3, calculates the response of a shelter to thermal loads and inlet air conditions. The manual explains the various features of the code, presents the I/O formats, gives sample data values and includes a typical application.
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General American Transportation Corporation, Niles, Ill.
SHELTER ENVIRONMENTAL PREDICTION (SHEP) COMPUTER CODE,
MODIFICATION 3
OCD Work Unit 1215A
Final Report 1423 (UNCLASSIFIED)
by C. E. Rathmann, R. J. Baschiere
June, 1968, pp. 108

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ENVIRONMENT, CONFINED ENVIRONMENTS, FALLOUT SHELTERS, COMPUTERS, PROGRAMMING (COMPUTERS)