

NASA Contractor Report 165982

NASA-CR-165982  
19830002292

NECAP 4.1 - NASA'S ENERGY COST ANALYSIS PROGRAM -  
THERMAL RESPONSE FACTOR ROUTINE

Michael R. Wiese  
*Computer Sciences Corporation*  
*Hampton, Virginia*

Prepared for  
Langley Research Center  
under Contract NAS1-16078  
August 1982



NF02104

**LIBRARY COPY**

SEP 21 1982

LANGLEY RESEARCH CENTER  
LIBRARY, NASA  
HAMPTON, VIRGINIA



National Aeronautics and  
Space Administration

Langley Research Center  
Hampton, Virginia 23665

## FOREWORD

This manual, which documents the THERMAL RESPONSE FACTOR ROUTINE (RESFAC - version 2) used by NASA'S ENERGY COST ANALYSIS PROGRAM (NECAP), is a suppliment to the NECAP ENGINEERING MANUAL (TM 83240) and the NECAP ENGINEERING FLOWCHARTS MANUAL (TM 83242).

The calculation sequences and flowcharts are given in the same format that is used by the NECAP ENGINEERING MANUAL and the NECAP ENGINEERING FLOWCHARTS MANUAL.

This version of RESFAC is the result of modifications and enhancements made to the original RESFAC. Although the RESFAC programming code has changed, the way in which the routine is accessed and used by NECAP is still the same. Therefore, the RESFAC usage information presented in the NECAP INPUT MANUAL (TM 83239) and the NECAP USERS MANUAL (TM 83238) is still accurate.

TABLE OF CONTENTS

	Page
OBJECTIVE AND DESCRIPTION . . . . .	1
DEFINING THERMAL RESPONSE FACTORS . . . . .	2
ALGORITHMS . . . . .	4
RESFAC . . . . .	5
RESIDU . . . . .	10
ROOTS . . . . .	13
THREBS . . . . .	18
BMEQ . . . . .	21

## OBJECTIVE AND DESCRIPTION

The Response Factor Program (RESFAC2) generates the time series of heat transfer factors (called response factors) required to accurately determine the transient flow of heat into, through, and out of interior/exterior building surfaces as they react to temperature differences across them.

These response factors are a function of the type of materials used and their order of placement in the surface. It is required that the following material properties be known for each material layer:

for non-air layer-

1. XL, thickness (FT)
2. XK, thermal conductivity (BTU/HR-FT-°F)
3. D, density (LB/FT<sup>3</sup>)
4. SH, specific heat (BTU/LB-°F)

for air layer-

5. RES, resistivity (HR-FT<sup>2</sup>-°F/BTU)

The sequencing of each layer's material characteristics is important. It must follow the way the surface is layered from the outside material to the inside.

## DEFINING THERMAL RESPONSE FACTORS

Thermal response factors can be defined as time dependent heat transfer coefficients which depict an object's action upon a particular outside surface/inside surface temperature difference over a period of time. This action is composed of three terms--the X, Y, and Z response factors.

Using the heat flux equation  $Q = U * \Delta T$  along with the response factors, the time dependent heat flux values for the planar construction shown in Figure 1 can be obtained.

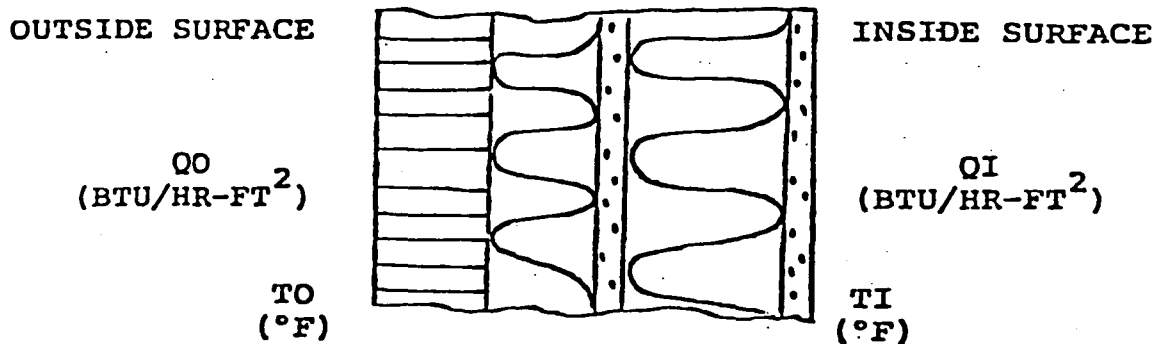


FIGURE 1

The outside surface heat flux ( $QO$ ) at any time  $t$  is calculated by :

$$QO_t = \sum_{i=0}^{NRT} (TO_{t-i} * X_i) - \sum_{i=0}^{NRT} (TI_{t-i} * Y_i)$$

where NRT is the number of response factor terms calculated,  $TO_{t-i}$  and  $TI_{t-i}$  are outside surface and inside surface temperatures at times  $t-i$  hour.

The inside surface heat flux (QI) at any time t is calculated by :

$$QI_t = \sum_{i=0}^{NRT} (TO_{t-i} * Y_i) - \sum_{i=0}^{NRT} (TI_{t-i} * Z_i)$$

In order for the steady state heat conduction situation

$$QO_t = QI_t = U(TO - TI)$$

$$TO = TO_t \quad \text{for any time } t$$

$$TI = TI_t \quad \text{for any time } t$$

to be satisfied, the individual summation of the X, Y, and Z response factors must equal the overall heat transfer coefficient U :

$$U = \left| \sum_{i=1}^{\infty} X_i \right| = \left| \sum_{i=1}^{\infty} Y_i \right| = \left| \sum_{i=1}^{\infty} Z_i \right|$$

## ALGORITHMS

The new Response Factor Program is comprised of five program modules:

Main program - RESFAC

Subroutines - RESIDU, ROOTS, and THREBS

Function - BMEQ

The following pages present input/output, calculation sequences, and flowcharts for each of these modules.

## RESFAC

A program which determines the thermal response factors for a particular roof, wall, or floor construction.

### INPUT

- M : number of material layers
- XL : thickness of each layer (FT)  
if air layer then XL = 0.0
- XK : thermal conductivity of each layer (BTU/HR-FT-<sup>o</sup>F)  
if air layer then XK = 0.0
- D : density of each layer (LB/FT<sup>3</sup>)  
if air layer then D = 0.0
- SH : specific heat of each layer BTU/Lb-<sup>o</sup>F)  
if air layer then SH = 0.0
- RES : thermal resistance of each AIR layer  
(HR-FT<sup>2</sup>-<sup>o</sup>F/BTU)  
if non-air layer then RES = 0.0
- DEFC : alpha-numeric description of each layer,  
maximum of 30 characters

### OUTPUT

- RFX }  
RFY } : Response factors series  
RFZ }
- NRFT : number of response factor terms
- R1 : common ratio

### CALCULATION SEQUENCE

1. Read number of material layers M
2. For i = 1, M
  - a) read and echo
    - 1) thickness XL<sub>i</sub>
    - 2) conductivity XK<sub>i</sub>
    - 3) density D<sub>i</sub>
    - 4) specific heat SH<sub>i</sub>



- 5) resistance  $RES_i$
  - 6) alpha-numeric description  $DEFC_i$
- b) for each non-air layer, calculate:
- 1) its resistance  $R_i = XL_i / XK_i$
  - 2)  $BETA_i = XL_i * SQRT(D_i * SH_i / XK_i)$
- c) for each air layer:
- 1) set  $R_i = RES_i$
  - 2)  $BETA_i = 0.0$
3. Call subroutine RESIDU to compute the thermal conductance  $RK0$  and the derivatives of matrix elements  $A$ ,  $B$ , and  $D$  (variables  $RK1$ ,  $RM1$ , and  $RM4$ ) for the condition where  $P$ , of  $B(P)$ , approaches  $0.0$
  4. Call subroutine ROOTS to calculate the roots of  $B(P) = 0.0$  and the number of roots  $NRT$
  5. For  $i = 1, NRT$ 
    - 1) call subroutine THREBS to calculate matrix elements  $A$ ,  $D$  and the derivative of matrix element  $B$  (variables  $B1$ ,  $B2$ , and  $BP3$ )
    - 2) set  $RKK(i,2) = 1.0 / BP3 / ROOT(i)^2$   
 $RKK(i,1) = RKK(i,2) * B1$   
 $RKK(i,3) = RKK(i,2) * B2$
  6. For  $i = 1, 100$ :
    - a) for  $j = 1, NRT$ :  
 if  $(ROOT(j) > 30.0)$  go to 6b  
 $BETAY = EXP(-ROOT(j) * i)$   
 $A = A + RKK(j,1) * BETAY$   
 $B = B + RKK(j,2) * BETAY$   
 $C = C + RKK(j,3) * BETAY$
    - b)  $A = A + RK1 + (RM4 * RK0) + (i * RK0)$   
 $B = B + (i * RK0) + RK1$   
 $C = C + RK1 + (RM1 * RK0) + (i * RK0)$
    - c) if  $(i = 1)$ :  
 $AA = A$   
 $BB = B$   
 $CC = C$

```

d)  if (.i = 2):
    AA = A-2.0*X
    BB = B-2.0*Y
    CC = C-2.0*Z

e)  if ( > 2):
    AA = A-2.0*X + FA
    BB = B-2.0*Y + FB
    CC = C-2.0*Z + FC

f)  set and echo response factors:
    RFX(i) = AA
    RFY(i) = BB
    RFZ(i) = CC

g)  if (i < 3) go to 6k

h)  if (ABS(XX/FAA-AA/XX) > 1.0E-5) go to 6k

i)  if (ABS(YY/FBB-BB/YY) > 1.0E-5) go to 6k

j)  if (ABS(ZZ/FCC-CC/ZZ) < 1.0E-5) go to 7

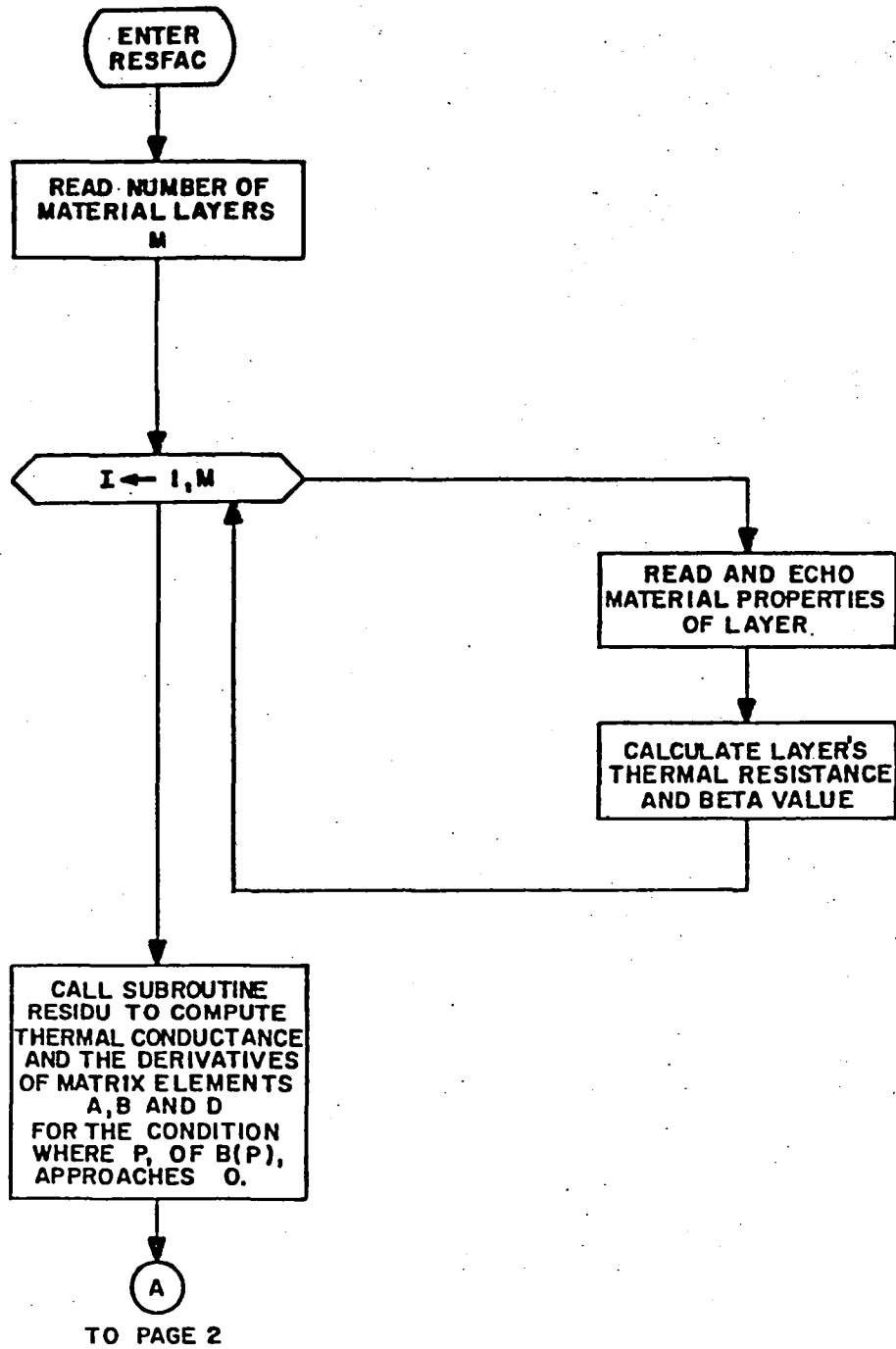
k)  if (ABS(AA) < 1.0E-8) go to 7

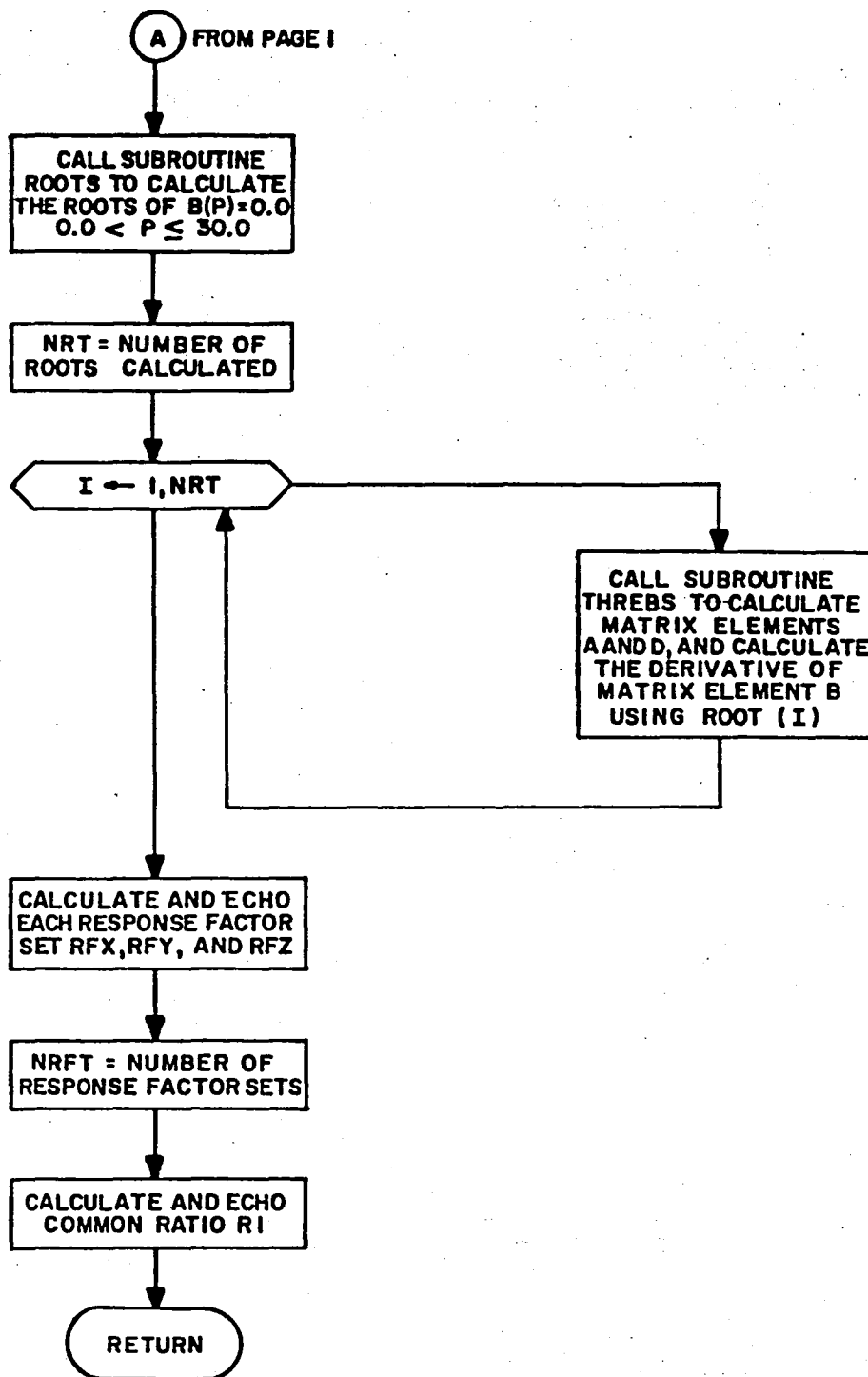
l)  set:
    FA = X
    FB = Y
    FC = Z
    FAA = XX
    FBB = YY
    FCC = ZZ
    XX = AA
    YY = BB
    ZZ = CC
    X = A
    Y = B
    Z = C
    go to 6

```

7. Set and echo common ratio:  
 $R1 = \text{EXP}(-\text{ROOT}(1))$

8. End





## RESIDU

A subroutine which determines thermal conductance and the derivatives of matrix elements A, B, and D for the condition where the root W approaches 0.0.

### INPUT

RR : each layers resistance  
BETA : each layers BETA  
M : number of layers

### OUTPUT

RK0 : thermal conductance  
RK1 : derivative of matrix element B  
RM1 : derivative of matrix element A  
RM4 : derivative of matrix element D

### CALCULATION SEQUENCE

1. Sum all layer resistances and compute thermal conductance  $RK0 = 1.0/R$  total
2. For  $i = 1, M$ 
  - a)  $P = BETA(1)*BETA(1)$   
 $R = RR(1)$
  - b) if ( $i > 1$ ):  
 $A = 1.0$   
 $B = R$   
 $C = 0.0$   
 $D = 1.0$   
go to 2e
  - c) if ( $i = 1$ ):  
 $A = P/2.0$   
 $B = R*P/6.0$   
 $C = P/R$   
 $D = P/2.0$
  - d) if ( $M = 1$ ):  
 $RM1 = A$   
 $RK1 = -RK0*RK0*B$   
 $RM4 = D$   
go to 4

```

e)  for j = 2, M
      1)  P = BETA(j)*BETA(j)
          R = RR(j)
          if i = j go to 2e2
          AA = 1.0
          BB = R
          CC = 0.0
          DD = 1.0
          go to 2f

      2)  AA = P/2.0
          BB = P*R/6.0
          CC = P/R
          DD = P/2.0

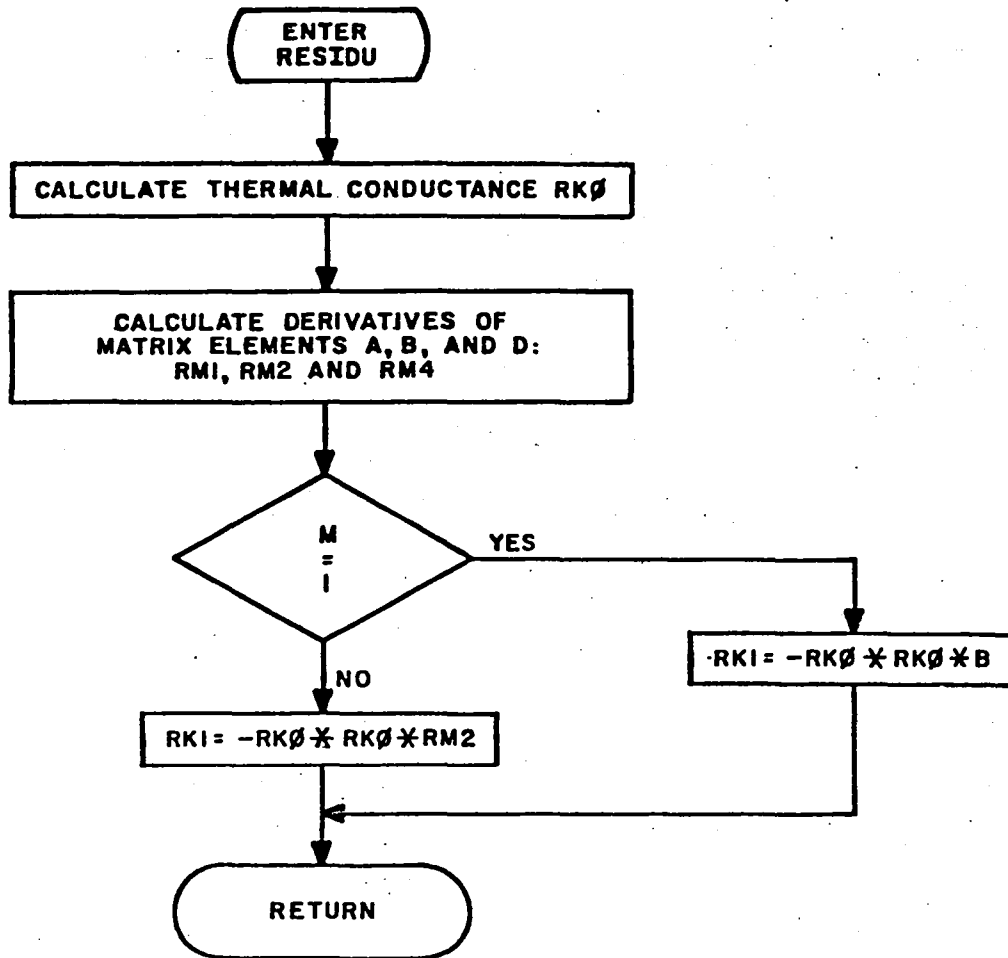
f)  F1 = A*AA+B*CC
     F2 = A*BB+B*DD
     F3 = C*AA+D*CC
     F4 = C*BB+D*DD
     A = F1
     B = F2
     C = F3
     D = F4
     go to 2e

g)  RM1 = RM1+F1
     RM2 = RM2+F2
     RM4 = RM4+F4
     go to 2

3.  RK1 = -RK0*RK0*RM2

4.  End

```



## ROOTS

A subroutine which determines the roots of matrix element  
 $B(P) = 0.0$

### INPUT

BTA       : each layers BETA  
RS        : each layers resistance  
N         : number of material layers

### OUTPUT

ROT       : root array  
L         : number of roots

### CALCULATION SEQUENCE

1. Set  $PI = 3.141592654$
2. For  $i = 1, N$ :
  - a) if  $BTA(i) > 0.0$  then calculate the zero points of this layers sine and cosine components:
    - 1) set  $R = 1.0$
    - 2) for  $j = 1, 99, 2$   
 $BM(j, i) = (R - 0.5) * PI / BTA(i)$   
 $BM(j + 1, i) = R * PI / BTA(i)$   
 $R = R + 1.0$
3. For values  $> 0.0$ , sort the BM arrays' values into the possible root interval array PINT in ascending order.
4. For  $i = 1, 1000$  determine the roots such that no root  $> 30.0$ :
  - a) set  $G1 = PINT(i)$  and calculate  $F1(G1)$  using function BMEQ
    - 1) if  $(ABS(F1) < 1.0E-8)$  go to 4e
  - b) set  $G2 = PINT(i + 1)$  and calculate  $F2(G2)$  using function BMEQ
    - 1) if  $(ABS(F2) < 1.0E-8)$  go to 4e
  - c) set the interval length  $D = G2 - G1$



d) sectionalize each interval into 1/10th segments and check each segment to determine if there is a root there:

- 1)  $FK = FK + 1.0$   
if  $(FK > 10.0)$  go to 4
- 2) set  $DD = PINT(i) + (D*FK/10.0)$  and  
calculate  $FD(DD)$  using function BMEQ
- 3)  $SM = FD*F1$   
if  $(SM \leq 0.0)$  go to 4d5
- 4)  $G1 = DD$   
 $F1 = FD$   
go to 4d1
- 5)  $GX = G1$   
 $FX = F1$   
 $G2 = DD$   
 $F2 = FD$   
go to 4f

e)  $L = L + 1$

- 1) if  $(ABS(F1) \leq 1.0E-8)$   $ROT(L) = G1**2$
- 2) if  $(ABS(F2) \leq 1.0E-8)$  and  $ROT(L) = 0.0)$   
 $ROT(L) = G2**2$
- 3) if  $(ROT(L) > 30.0)$  go to 5  
else go to 4

f) use secant method to find root

- 1)  $G3 = G2 - (F2*(G2-G1)/(F2-F1))$
- 2) if  $(G3 < GX)$  or  $(G3 > DD)$  then secant method fails  
so use bisection method to locate root - go to g
- 3) if  $(G3 > GX)$  and  $(G3 < DD)$  then calculate  $FRT(G3)$   
using function BMEQ
- 4) if  $(ABS(FRT) \leq 1.0E-8)$  go to 4j
- 5)  $G1 = G2$   
 $G2 = G3$   
 $F1 = F2$   
 $F2 = FRT$   
go to 4f1

```

g) set  $G4 = 0.5 * (G1 + G2)$  and calculate
    $F4(G4)$  using function BMEQ

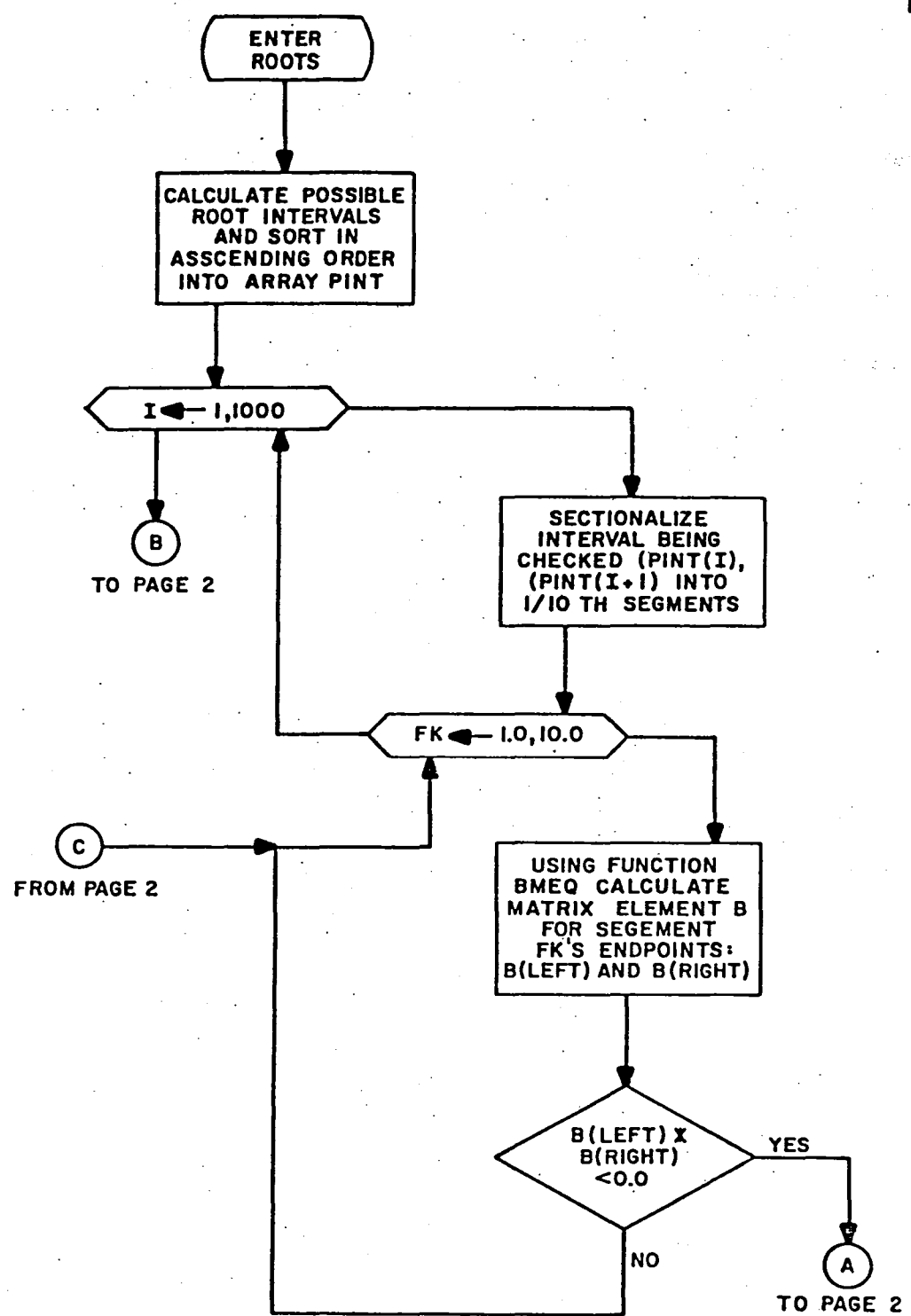
h) if  $(ABS(F4) \leq 1.0E-8)$   $G3 = G4$ 
   1) go to 4j

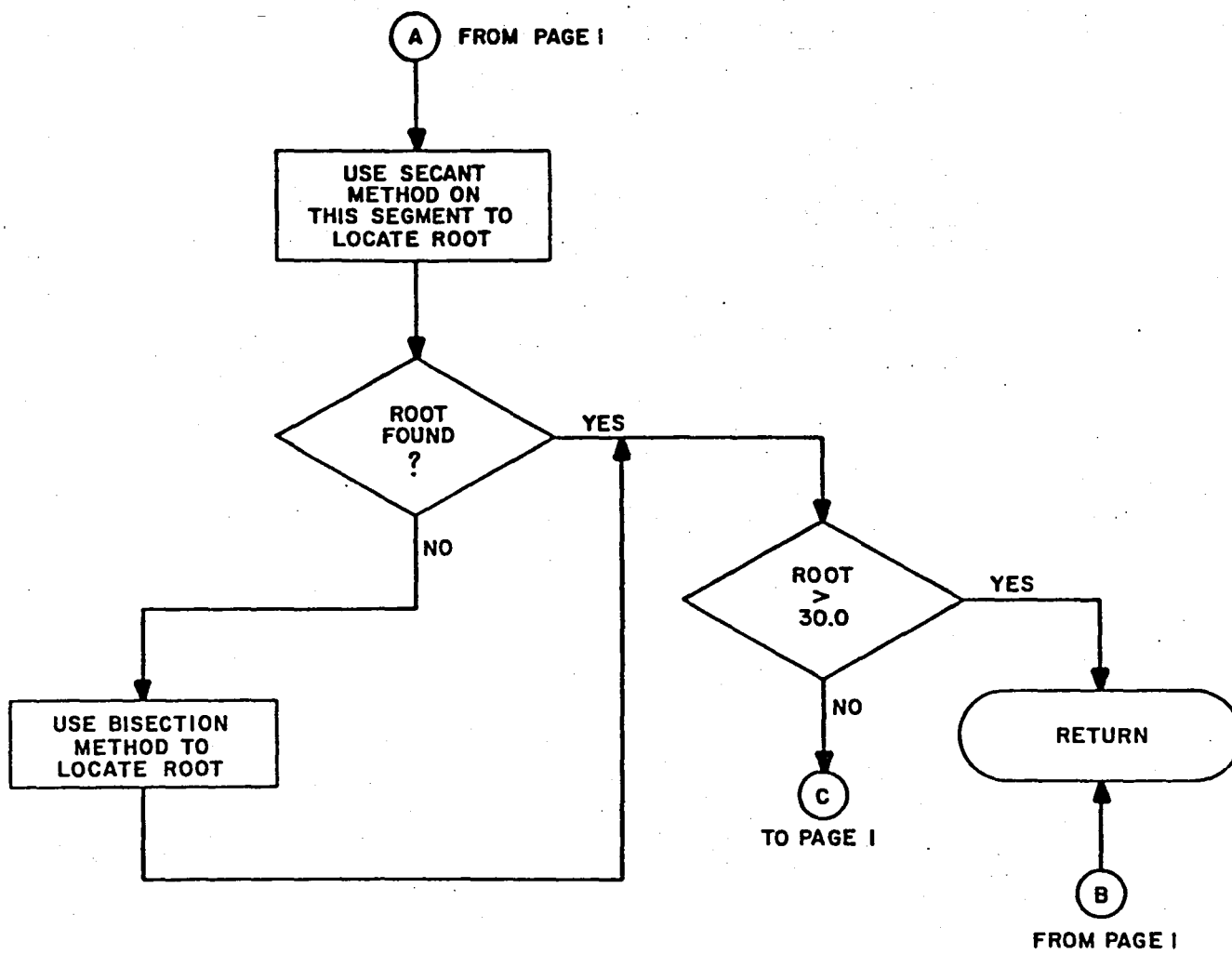
i)  $F5 = F1 * F4$ 
   if  $(F5 < 0.0)$   $G2 = G4$ 
   if  $(F5 > 0.0)$   $G1 = G4$  and  $F1 = F4$ 
   go to 4g

j)  $L = L + 1$ 
    $ROT(L) = G3 ** 2$ 
   if  $(ROT(L) > 30.0)$  go to 5
    $G1 = DD$ 
    $F1 = FD$ 
   go to 4dl

5) End

```





## THREBS

A subroutine which determines matrix elements A, D, and the derivative of matrix element B at the root W.

### INPUT

RR : each layers resistance  
BETA : each layers BETA  
W : root  
M : number of layers

### OUTPUT

B1 : matrix element A  
B2 : matrix element D  
BP3 : derivative of matrix element B

### CALCUALTION SEQUENCE

1. For i = 1, M
  - a)  $P = \text{SQRT}(W) * \text{BETA}(i)$   
 $R = \text{RR}(i)$   
 $\text{ALPHA} = \text{BETA}(i)$   
 $\text{SQ} = \text{SQRT}(W)$
  - b) if (P = 0.0):  
 $\text{AL}(i) = 1.0$   
 $\text{BL}(i) = R$   
 $\text{CL}(i) = 0.0$   
 $\text{DAL}(i) = 0.0$   
 $\text{DBL}(i) = 0.0$   
 $\text{DCL}(i) = 0.0$
  - c) if (P > 0.0):  
 $\text{AL}(i) = \text{COS}(P)$   
 $\text{BL}(i) = R/P * \text{SIN}(P)$   
 $\text{CL}(i) = -P/R * \text{SIN}(P)$   
 $\text{DAL}(i) = \text{ALPHA} * \text{SIN}(\text{ALPHA} * \text{SQ}) / 2.0 / \text{SQ}$   
 $\text{DBL}(i) = -R * \text{COS}(\text{ALPHA} * \text{SQ}) / 2.0 / W + R * \text{SIN}(\text{ALPHA} * \text{SQ}) / \text{ALPHA} / 2.0 / \text{SQ} / \text{SQ} / \text{SQ}$   
 $\text{DCL}(i) = \text{ALPHA} * \text{ALPHA} * \text{COS}(\text{ALPHA} * \text{SQ}) / 2.0 / R + \text{SIN}(\text{ALPHA} * \text{SQ}) / 2.0 / \text{SQ} * \text{ALPHA} / R$
  - d) go to 1

```

2.  If (M = 1):
    BP3 = DBL(1)
    B1 = DAL(1)
    B2 = AL(1)
    go to 7

3.  For i = 1, M
    a)  DA = 1.0
        DB = 0.0
        DTA = 0.0
        DTB = 0.0

    b)  for j = 1, M
        1)  if (i = j):
            DTA = (DA*DAL(j)) + (DB*DCL(j))
            DTB = (DA*DBL(j)) + (DB*DAL(j))
            go to 3b3

        2)  DTA = (DA*AL(j)) + (DB*CL(j))
            DTB = (DA*BL(j)) + (DB*AL(j))

        3)  DA = DTA
            DB = DTB
            go to 3b

    c)  BP3 = BP3 + DTB

    d)  go to 3

4.  A = AL(1)
    B = BL(1)
    C = CL(1)
    D = AL(1)

5.  For i = 2, M
    a)  TA = (A*AL(i)) + (B*CL(i))
        TB = (A*BL(i)) + (B*AL(i))
        TC = (C*AL(i)) + (D*CL(i))
        TD = (C*BL(i)) + (D*AL(i))
        A = TA
        B = TB
        C = TC
        D = TD

    b)  go to 5

6.  B1 = TD
    B2 = TA

7.  End

```

## BMEQ

A function which determines the matrix element B at the root guess W.

### INPUT

W : root guess  
BETA : each layers BETA  
R : each layers resistance  
M : number of layers

### OUTPUT

BMEQ : matrix element B

### CALCULATION SEQUENCE

1. For  $i = 1, M$ 
  - a) if (BETA(i) = 0.0):  
AL(i) = 1.0  
BL(i) = R(i)  
CL(i) = 0.0  
to to 1
  - b)  $P = W * BETA(i)$   
AL(i) = COS(P)  
SN = SIN(P)  
BL(i) = R(i) \* SN / P  
go to 1
2. If (M = 1):  
TB = BL(1)  
go to 5
3. A = AL(1)  
B = BL(1)
4. For  $i = 2, M$   
TA = (A \* AL(i)) + (B \* CL(i))  
TB = (A \* BL(i)) + (B \* AL(i))  
A = TA  
B = TB
5. BMEQ = TB
6. End

1. Report No. NASA CR-165982		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle NECAP 4.1 - NASA'S ENERGY COST ANALYSIS PROGRAM - THERMAL RESPONSE FACTOR ROUTINE				5. Report Date August 1982	
				6. Performing Organization Code	
7. Author(s)  Michael R. Wiese				8. Performing Organization Report No.	
9. Performing Organization Name and Address  Computer Sciences Corporation Hampton, Virginia				10. Work Unit No.	
				11. Contract or Grant No.  NAS1-16078	
12. Sponsoring Agency Name and Address  National Aeronautics and Space Administration Washington, D.C. 20546				13. Type of Report and Period Covered Contractor Report 1981-1982	
				14. Sponsoring Agency Code	
15. Supplementary Notes  Langley Technical Monitors: John E. Hogge and Ronald N. Jensen					
16. Abstract  The RESFAC2 version of the Thermal Response Factor Program (RESFAC) is the result of numerous modifications and additions to the original RESFAC. These modifications and additions have significantly reduced the program's computational time requirement. As a result of this work, the program is more efficient and its code is both readable and understandable.  This report describes what a thermal response factor is and provides calculation sequences and flowcharts for RESFAC2.  RESFAC is used by NASA'S ENERGY COST ANALYSIS PROGRAM (NECAP) to calculate hourly heat transfer coefficients (thermal response factors) for each unique delayed surface. NECAP uses these response factors to compute each spaces' hourly heat gain/loss.					
17. Key Words (Suggested by Author(s))  ENERGY ENERGY ANALYSIS HEAT TRANSFER			18. Distribution Statement  Subject Category 44 Unclassified-Unlimited		
19. Security Classif. (of this report)  Unclassified	20. Security Classif. (of this page)  Unclassified	21. No. of Pages  26	22. Price  A03		



**End of Document**